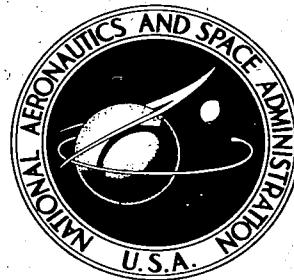


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TEMPERATURE, PRESSURE, DENSITY,
AND WIND MEASUREMENTS WITH THE
ROCKET GRENADE EXPERIMENT, 1960-1963

by *W. Smith, L. Katchen, P. Sacher,
P. Swartz, and J. Theon*

*Goddard Space Flight Center
Greenbelt, Md.*

NATIONAL AERONAUTICS AND SPACE ADMINISTRATION • WASHINGTON, D. C. • OCTOBER 1964

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SUMMARY

Complete data from 28 rocket grenade experiments at Wallops Island, Virginia, and Fort Churchill, Canada, are presented. Pressures, temperatures, densities, and winds have been derived directly from the recorded times of explosions and sound arrivals; but no attempt has been made to analyze the meteorological significance of these measurements. Error analyses on 16 of the Wallops experiments are also included.



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INTRODUCTION

During the period 1960-1963, a total of 28 rocket grenade experiments were carried out by Goddard Space Flight Center at Wallops Island, Virginia, and Fort Churchill, Canada. It is the purpose of this report to present the complete data from these experiments. The data have been reduced but not analyzed, i.e., the physical measurements (pressure, density, temperature and winds) have been derived directly from recordings of the times of grenade explosions and sound arrivals, and from the rocket trajectories; but no attempt has been made to analyze the measurements for their meteorological significance. Rather, this report should be considered as a record of the unsmoothed, raw measurements which may serve as the basis of further investigation and interpretation of the structure of the atmosphere. This is the first such report since the program started in 1960. As the program continues, future results will be documented in similar fashion.

The grenade experiment is one of the several techniques employed in NASA's Meteorological Rocket Sounding Program, the objective of which is to obtain as representative as possible a sample of the synoptic structure of the mesosphere and lower ionosphere. In order to extend the findings over the widest possible geographic area, and perhaps eventually to attain a global network of soundings, the NASA launchings are coordinated whenever possible with soundings in other parts of the world. The instrumental details and methods of data reduction have been thoroughly described elsewhere.*

EXPERIMENTAL METHOD

One and two pound explosive charges (grenades) are carried aloft in the nosecone of a Nike-Cajun sounding rocket. The grenades are ejected and exploded at 4-6 km intervals. Either a precise radar such as the FPS-16 or a doppler tracking system, or both, are used to determine the

* Nordberg, W., and Smith, W., "The Rocket Grenade Experiment," NASA Technical Note D-2107, March 1964.

rocket position and hence the exact position of the explosion. The time of the explosion is detected by small rocket borne infrared photocells and telemetered to the ground. A ground based array of hot wire microphones with frequency response peaked at 4 cycles per second is used to detect and record the sound waves from each exploding grenade. The measured experimental parameters are the times of the grenade explosions, the positions of the grenade explosions, and the times of arrival of the sound waves at the ground based microphones.

Elevation and azimuth angles are computed for each arriving sound wave front by applying a least-squares fit to the arrival times at the various microphones. Each wave is then analytically traced up through the atmosphere by means of Snell's law. Data from radiosonde ascents or from small meteorological rockets obtained at the time of the grenade soundings are used for this tracing up to the first explosion; above this, the results of the experiment itself are used for each successive explosion. This *apparent* position of the *wave* is then compared with the *known* position of the *wave source*, the grenade explosion. The amount by which the sound wave has been displaced horizontally from one explosion to the next is a measure of the average wind velocity vector in the layer between any two adjacent explosions. The average speed of the sound, and hence average temperature between two adjacent explosions, may also be determined. This analysis yields an altitude profile of temperatures and winds as a direct measurement. The temperature profile consists of discrete points, each representing an average value for an altitude layer between grenade explosions. It may be used to derive density and pressure profiles, if the pressure or density is known at a given level at the bottom of the temperature profile; and the latter data are available from the accompanying radiosonde. Pressure is calculated by use of the hydrostatic equation, and the ideal gas law; an integration is performed over the temperature profile starting at the known pressure. The density at any level is then computed from the pressure, temperature, and universal gas constant.

During the period between July 8, 1960 and December 7, 1963, 23 successful rocket grenade soundings were conducted from Wallops Island, Virginia ($37^{\circ} 50'N$, $75^{\circ} 29'W$). In addition to offering excellent launch and tracking support, the geographical location of Wallops Island makes it a good middle-latitude observation site. Five soundings were conducted from a sub-arctic range, Fort Churchill, Canada, ($58^{\circ} 47'N$, $94^{\circ} 17'W$) in the period between December 1962 and March 1963. Originally, it was planned to distribute the number of firings about equally between the two sites, but a fire early in 1961 destroyed part of the Fort Churchill launch facility, and it was not operational again until November 1962. Table 1 lists the soundings conducted. Four of the recent firings from each site were conducted nearly simultaneously.

The results of the 28 soundings are presented in Figures 1 through 43. In Figures 1 through 28, the *directly measured* parameters of temperatures and winds are tabulated (actual computer printouts) in the columns on the left side of the page immediately above the graph. Tables of pressure and density *derived* from the temperature profiles are also shown. The temperatures were linearly interpolated between each of the measured points.

Table 1

Dates, Times, and Locations of GSFC Grenade Experiments 1960-1963

Date	Local Time	Location
8 July 1960	2259	Wallops Island
14 February 1961	1850	Wallops Island
16 February 1961	2126	Wallops Island
5 April 1961	0757	Wallops Island
5 May 1961	1800	Wallops Island
5 May 1961	2354	Wallops Island
13 July 1961	1707	Wallops Island
14 July 1961	1102	Wallops Island
20 July 1961	0530	Wallops Island
16 September 1961	1855	Wallops Island
1 March 1962	1901	Wallops Island
2 March 1962	0615	Wallops Island
23 March 1962	1854	Wallops Island
27 March 1962	1904	Wallops Island
17 April 1962	0428	Wallops Island
6 June 1962	2005	Wallops Island
7 June 1962	2053	Wallops Island
1 December 1962	1625	Wallops Island
4 December 1962	0105	Fort Churchill
6 December 1962	0032	Wallops Island
5 December 1962	2343	Fort Churchill
20 February 1963	1734	Fort Churchill
20 February 1963	1847	Wallops Island
28 February 1963	1547	Fort Churchill
28 February 1963	1711	Wallops Island
8 March 1963	1901	Wallops Island
8 March 1963	1801	Fort Churchill
7 December 1963	0812	Wallops Island

Winds and temperatures below 30 km obtained from radiosondes, and below 50 km from smaller meteorological sounding rockets (Arcas* and Hasp† whenever available) launched nearly simultaneously with the grenade soundings are shown graphically. Winds and temperatures above 40 km from the grenade soundings are shown on the graph.

RESULTS

In the results from these soundings all data points, regardless of our degree of confidence, are presented in tabular form. Some individual data points may be subject to later revision, as there may be occasional errors in some of the records which have not yet been detected. In the

* "Data Report of the Meteorological Rocket Network, Spring 1961 Firings," U.S. Army Signal Missile Agency, White Sands Missile Range, New Mexico, September 1961.

† Private Communication from M. J. Parker, Naval Ordnance Laboratory, White Oak, Maryland.

preparation of these graphs some data points, where such errors seem obvious, were omitted and the graphs note the omissions. For the most part, these occur at the upper altitude limit of the experiment where the signal-to-noise ratio of detected acoustic waves is poor. Random errors contained in either the measurements or in the data reductions can usually be recognized by comparing two adjacent data points. Since these errors will generally be contained in the parameters (time and space coordinates of the explosion) associated with one individual grenade explosion, the temperature data points both below and above this explosion will contain errors of approximately equal magnitude but opposite sign. Therefore, if large excursions of this nature occur between two adjacent data points, it is very likely that the recordings from the explosion between these two data points were in error.

ERROR ANALYSIS

An error analysis was run with the aid of a digital computer on 16 of the 28 experiments reported. The firings considered were the first 16 conducted from Wallops Island. The following nomenclature is used in the error analysis:

Δ_w - Difference in west coordinate between successive grenade explosions.

Δ_n - Difference in north coordinate between successive grenade explosions.

h - Difference in altitude between successive grenade explosions.

ω - Wind direction in the layer.

w - Wind speed in the layer.

c - Speed of sound in the layer = $k(T)^{1/2}$, where k is a proportionality constant depending on molecular mass, the ratio of specific heats, and the universal gas constant.

ϕ_u - Azimuth angle of sound wave for upper explosion.

τ - Travel time of sound wave in layer.

K - $c_0 \sec \theta_u + w_0 \cos(\phi_u - \omega_0) - w \cos(\phi_u - \omega)$, where c_0 is the mean speed of sound over the microphone array; θ_u is the elevation angle of sound wave for upper explosion; w_0 is the wind speed over the microphone array; and ω_0 is the wind direction over the microphone array.

t - Travel time of sound wave from grenade explosion to ground.

T - Mean temperature in layer.

Δt - Time difference between microphones introduced by changing the time of arrival at one microphone.

θ'_u - Elevation angle from ground to apparent position of upper grenade explosion as obtained by ray tracing.

In order to determine the error function, deliberate errors were introduced in the following experimental parameters:

A. Position of grenade explosions

1. North: 200 meters
2. West: 200 meters
3. Up: 50 meters

B. Travel time of sound from explosions to ground: 0.3 second.

C. Time of arrival at one of the 6 microphones relative to the other five microphones: 0.02 second.

It was determined that an error in one of the foregoing parameters for any given grenade will cause wind and temperature errors in the two layers adjacent to the grenade. The temperature errors, in general, will be of opposite sign and approximately equal in magnitude. There are slight errors introduced in the remaining layers above the grenade; however, these are negligibly small. The errors in the temperatures and winds due to errors in the coordinates of the explosions are given by:

$$\frac{\partial W}{\partial \Delta w} = \frac{\sin \omega}{\tau}; \quad (1)$$

$$\frac{\partial W}{\partial \Delta n} = \frac{\cos \omega}{\tau}; \quad (2)$$

$$\frac{\partial W}{\partial h} = \frac{\cot \theta'_u}{\tau} \cos (\omega - \phi_u); \quad (3)$$

$$\frac{\partial c}{\partial \Delta w} = \frac{\sin \phi_u}{c \tau} \left[\frac{h^2 K}{\tau^2 (K^2 - 2c^2)} - \frac{c^2}{K} \right]; \quad (4)$$

$$\frac{\partial c}{\partial \Delta n} = \frac{\cos \phi_u}{c \tau} \left[\frac{h^2 K}{\tau^2 (K^2 - 2c^2)} - \frac{c^2}{K} \right]; \quad (5)$$

$$\frac{\partial c}{\partial h} = \frac{1}{c \tau} \left[\frac{h^2 K \cot \theta'_u - h K^2 \tau}{\tau^2 (K^2 - 2c^2)} + \frac{c^2 \cot \theta'_u}{K} \right]. \quad (6)$$

In the error analysis, the north and west coordinates of alternate grenades were changed by -200 m, and the up coordinates were changed by -50 m. This means that $d\Delta_w$ and $d\Delta_n$ for adjacent layers were alternatingly +200 and -200, and dh for adjacent layers were alternatingly +50 and

-50. The azimuth angle changes slowly with altitude. Generally, $\sin \phi_u$ and $\cos \phi_u$ do not change sign during an experiment; thus the signs of $(\partial c / \partial \Delta w) d\Delta w$ and $(\partial c / \partial \Delta n) d\Delta n$ alternate regularly from layer to layer *as the coordinates of alternate grenade explosions are changed*. This accounts for the regular alternation of the temperature error, since all other signs in the equation for $\partial c / \partial \Delta w$, $\partial c / \partial \Delta n$ remain constant during an experiment. Similarly, it can be seen from the expression for $\partial c / \partial h$ that all the quantities retain the same sign throughout an experiment. Thus, the same regular alternation for the signs of the $(\partial c / \partial h) dh$ will occur for successive grenades.

The situation is different, however, for $\partial W / \partial \Delta w$, $\partial W / \partial \Delta n$, $\partial W / \partial h$. The sign of $\partial W / \partial \Delta w$ depends on the sign of $\sin \omega$ which in turn depends on the value of ω . Since ω may vary from 0 to 360° , $\sin \omega$ may be either positive or negative. The same is true for the sign of $\partial W / \partial \Delta n$, which depends on $\cos \omega$. Hence, we expect no regular alternation from layer to layer in the sign of the wind error. The sign of $\partial W / \partial h$ depends on the sign of $\cos(\omega - \phi_u)$ which in turn depends on the value of $\omega - \phi_u$. Although ϕ_u changes slowly and in general remains in the same quadrant, ω can vary from 0 to 360° , and hence $\omega - \phi_u$ can be positive or negative. Thus, $(\partial W / \partial h) dh$ exhibits no *regular* alternation in sign. In summary, we can see that the signs of $\partial c / \partial \Delta w$, $\partial c / \partial \Delta n$, $\partial c / \partial h$ are constant and hence an error in the coordinates of one individual grenade explosion will cause a positive error in the measured temperatures in the layer below the explosion if a negative error is caused in the layer above the explosion, and vice versa. In general, the magnitudes of the temperature errors caused by an error of the explosion coordinates between two adjacent layers are approximately equal.

However, this does not hold for wind errors. The error functions for the wind speed are proportional to $\sin \omega$, $\cos \omega$ and $\cos(\omega - \phi_u)$, which may vary considerably from layer to layer. The error functions of c , however, are proportional to ϕ_u and θ'_u which do not vary greatly from layer to layer.

The two other parameters of importance to the errors in addition to the grenade explosion coordinates were investigated in a similar manner. These parameters were: the time differences, Δt , between arrival of the sound wave at any two microphones within the array of six; and the travel time, t , of the sound from the explosion to the ground. The parameter Δt is important because the direction of the arriving sound wave front is derived from those differences, while t enters primarily in the calculation of the speed of sound in the layer. An error of .02 second was introduced into the arrival time at one microphone without altering the arrival times at the remaining five microphones, while an error of .3 second was introduced into t . As in the case of the coordinates of the grenade explosions, these errors were introduced only for alternate grenades.

A typical result of the error analysis is presented in Figures 29 through 38. From a study of these figures, the following conclusions can be reached:

1. Relative errors in the North and West coordinates of 200 meters will significantly affect only winds by about 10 m/sec but not the temperatures.
2. Relative errors in the up coordinates of 50 meters will cause significant errors of about $5^\circ K$ in temperature, but not in winds.

3. An error of .3 second in t will give rise to large temperature errors - about 10°K - but in general only very small wind errors.
4. An error of .02 in the relative arrival times between microphones will cause the largest errors in both winds and temperatures: 10-40 m/sec and $10-25^{\circ}\text{K}$. The error analysis clearly shows that an error introduced into the input parameters of a grenade significantly affects only the layers adjacent to the particular grenade. No significant error is introduced into the calculated winds and temperature for succeeding grenades, and hence only the layers adjacent to the grenade in question need be considered.

Table 2 gives the average error functions for the 16 firings tabulated by layers. Figures 39 and 40 are graphs of the two functions which are most strongly altitude dependent, $\partial T/\partial \Delta t$ and $\partial W/\partial \Delta t$, showing quite clearly the increase of the error function with altitude.

Table 2
Absolute Average Error Functions

Layer	$t + .3 \text{ sec}$		North-200m		West-200m		Up-50m		$\Delta t + .02 \text{ sec}$	
	Temp. ($^{\circ}\text{K}$)	Wind (m/sec)								
1	10.1	.5	.9	3.9	.7	9.2	5.4	.8	11.7	12.2
2	10.2	.7	.9	5.3	.7	10.6	5.6	.6	15.2	18.5
3	13.0	1.0	.9	5.2	.8	11.9	6.7	.8	16.3	22.0
4	10.5	1.1	.6	4.6	.6	10.7	5.8	.6	17.8	22.3
5	8.4	.9	.4	2.5	.4	9.5	4.6	.5	12.0	16.9
6	7.7	1.0	.4	3.7	.5	8.7	4.5	.7	15.1	26.4
7	10.0	1.3	.4	6.0	.5	10.6	5.6	.8	16.3	25.3
8	9.2	1.2	.4	6.3	.7	10.3	5.6	.7	20.9	31.9
9	11.7	2.3	.5	5.8	.8	12.1	6.4	.8	21.4	30.5
10	8.3	2.4	.5	8.2	.8	9.3	5.4	.7	22.5	41.1
11	11.5	5.2	.4	9.8	.7	11.4	6.4	.5	22.4	35.2

Figure 41 shows the dependence of $\partial T/\partial \Delta t$ upon zenith angle. As the zenith angle increases, the error function increases nearly linearly. Thus, to make the experiments as accurate as possible, it is desirable that the sound propagation be as nearly vertical as possible. A zenith angle of 0° would, of course, be ideal; however, range safety considerations make this impossible, and at Wallops Island the zenith angles usually lie in the range from $15^{\circ} - 30^{\circ}$. The zenith angles at Fort Churchill are generally less than 10° , and the probable error in the Fort Churchill data is therefore correspondingly less.

The magnitudes of the errors assumed in this analysis were chosen arbitrarily large for convenience in calculation. The actual resulting errors will be much smaller, as will be shown below. The magnitude of the actual errors in the rocket grenade experiment is determined by multiplying the error functions $\partial W/\partial \Delta w$, $\partial W/\partial \Delta n$, $\partial W/\partial \Delta h$, etc., by the value of the actual errors in Δw , Δn , h , Δt , and t . The maximum error is calculated by summing all the partial errors:

$$\left(\frac{\partial W}{\partial \Delta w} d\Delta w + \frac{\partial W}{\partial \Delta n} d\Delta n + \frac{\partial W}{\partial \Delta h} d\Delta h + \dots \text{etc.} \right)$$

The actual errors in coordinates and times are estimated in the following manner:

The position of the grenade explosion is determined by two totally independent tracking methods, DOVAP and radar. The agreement of these two systems with regard to the coordinates Δn , Δw and h in general is better than 20 meters. The result is a maximum temperature error of 1°K and maximum wind error of 1-2 meters/sec, according to the error functions. The time of the grenade explosion, determined primarily by rocket borne infrared photocells, is telemetered to the ground equipment. The time of grenade explosions may also be determined by ground based flash detectors or radar signal strength records. It has been shown that this time can generally be determined within $\pm .001$ second. The errors in determining the arrival time of the sound at the ground range from $\pm .001$ to $\pm .010$ second. Thus, the maximum error expected in determining the travel time (t) of the sound between explosion and ground is approximately .01 second, which results in a temperature error of 0.3°K and virtually no errors in winds. By far the largest contribution to the total error comes from errors in Δt , which also range from .001 to .010 second, depending upon the background noise level and the altitude of the explosion. The error in Δt is obtained by determining typical discrepancies among a number of independent Δt readings for each explosion. These errors result in temperature errors ranging from 1°K at 40 km to 15°K at 90 km, and wind errors from 1 to 16 m/sec over the same altitude range.

The maximum errors in the 16 soundings considered in this error analysis are presented in Figures 42 and 43, which clearly show the increase of the maximum errors with altitude. This increase is to be expected, since the amplitude of the sound waves will decrease rapidly with increasing altitudes, making it difficult to distinguish the grenade explosion from the background noise level. Since the determination of the relative arrival times between microphones is by far the most critical measured parameter, the largest part of the maximum error is due to the attenuation of the sound wave with altitude.

ACKNOWLEDGMENTS

The authors greatly appreciate the contributions of: Superior Engineering Company in designing and constructing the payload instrumentation for the grenade experiment; Texas Western College in conducting the sound ranging portion of this experiment; and New Mexico State University in operating the DOVAP tracking system.

Manuscript received July 9, 1964.

Figures 1 through 28

**Graphs and tables of temperatures, winds, pressures,
and densities derived from 28 rocket grenade firings,
1960 - 1963.**

FIGURE 1
8 JULY 1960, 2259 EST, WALLOPS ISLAND, VA.

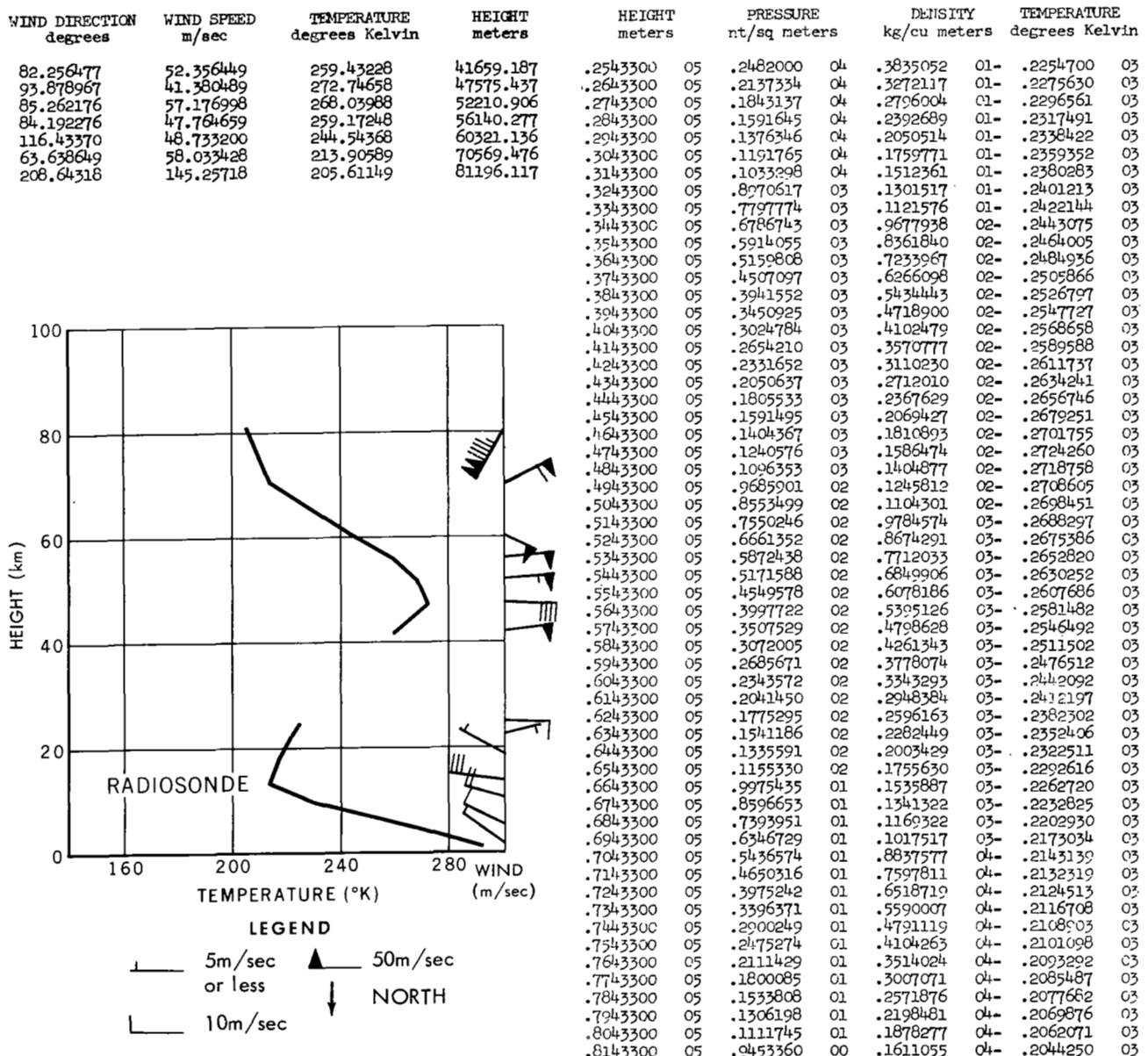


FIGURE 2
14 FEBRUARY 1961, 1850 EST, WALLOPS ISLAND, VA.

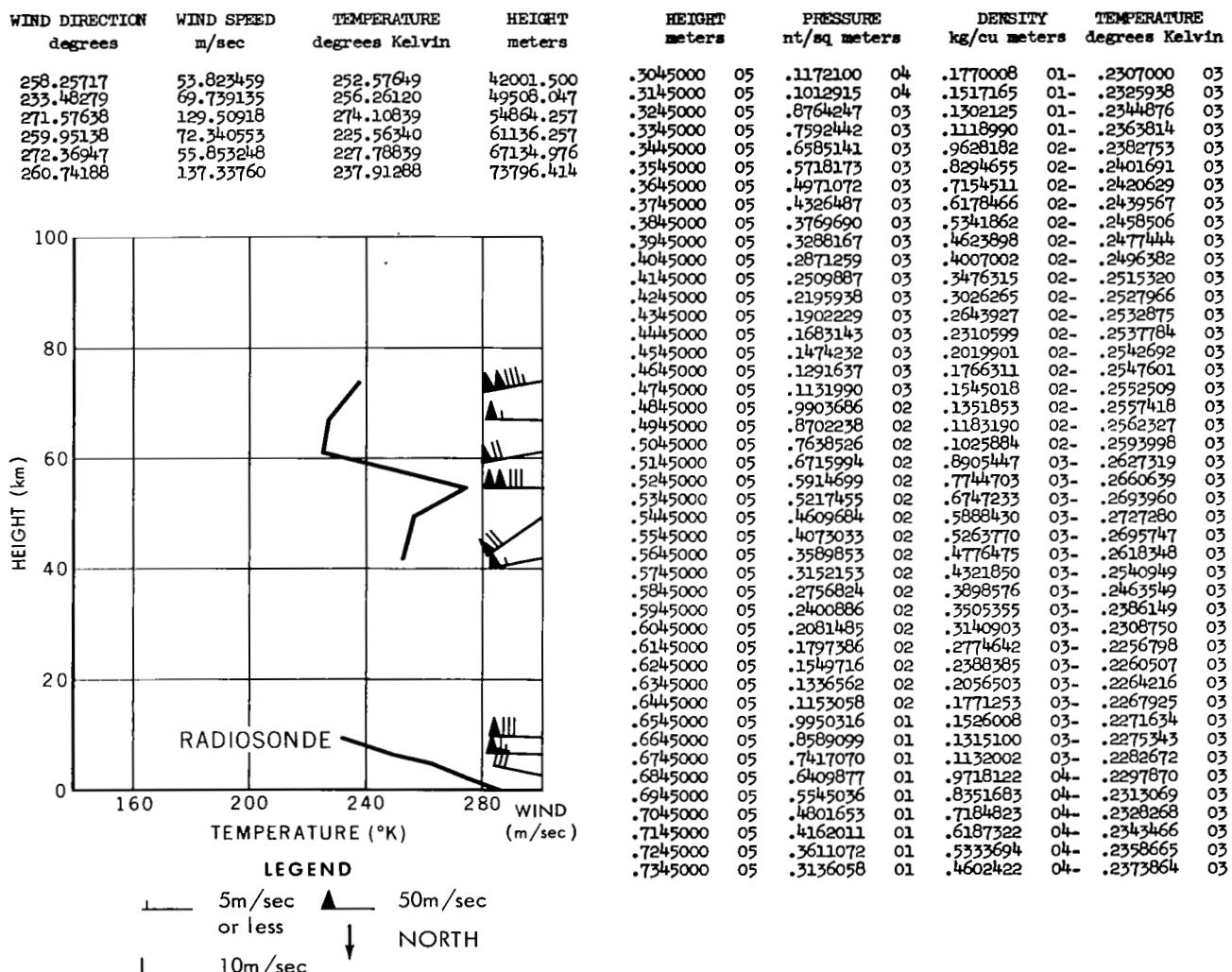


FIGURE 3
16 FEBRUARY 1961, 2126 EST, WALLOPS ISLAND, VA.

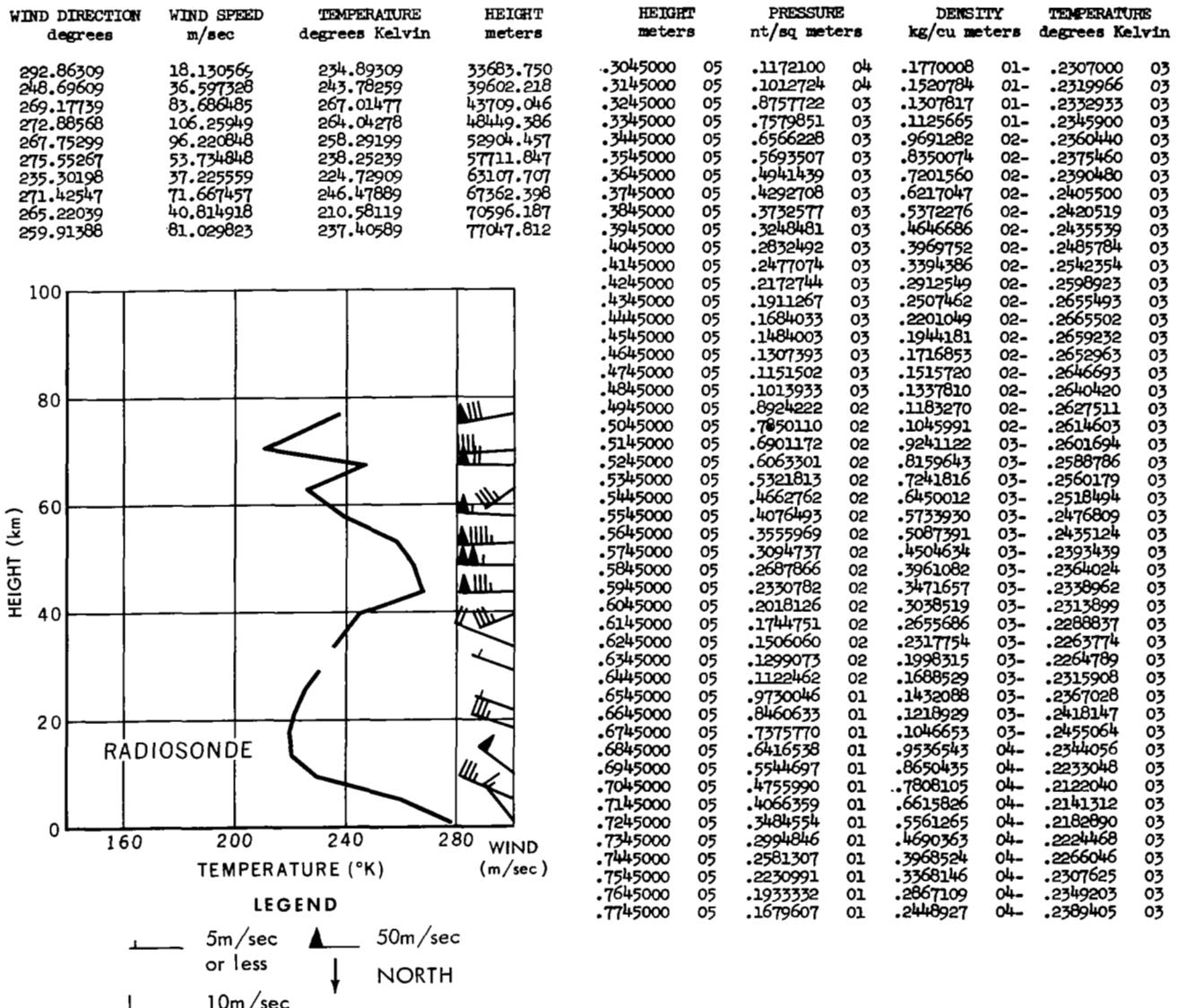


FIGURE 4
5 APRIL 1961, 0757 EST, WALLOPS ISLAND, VA

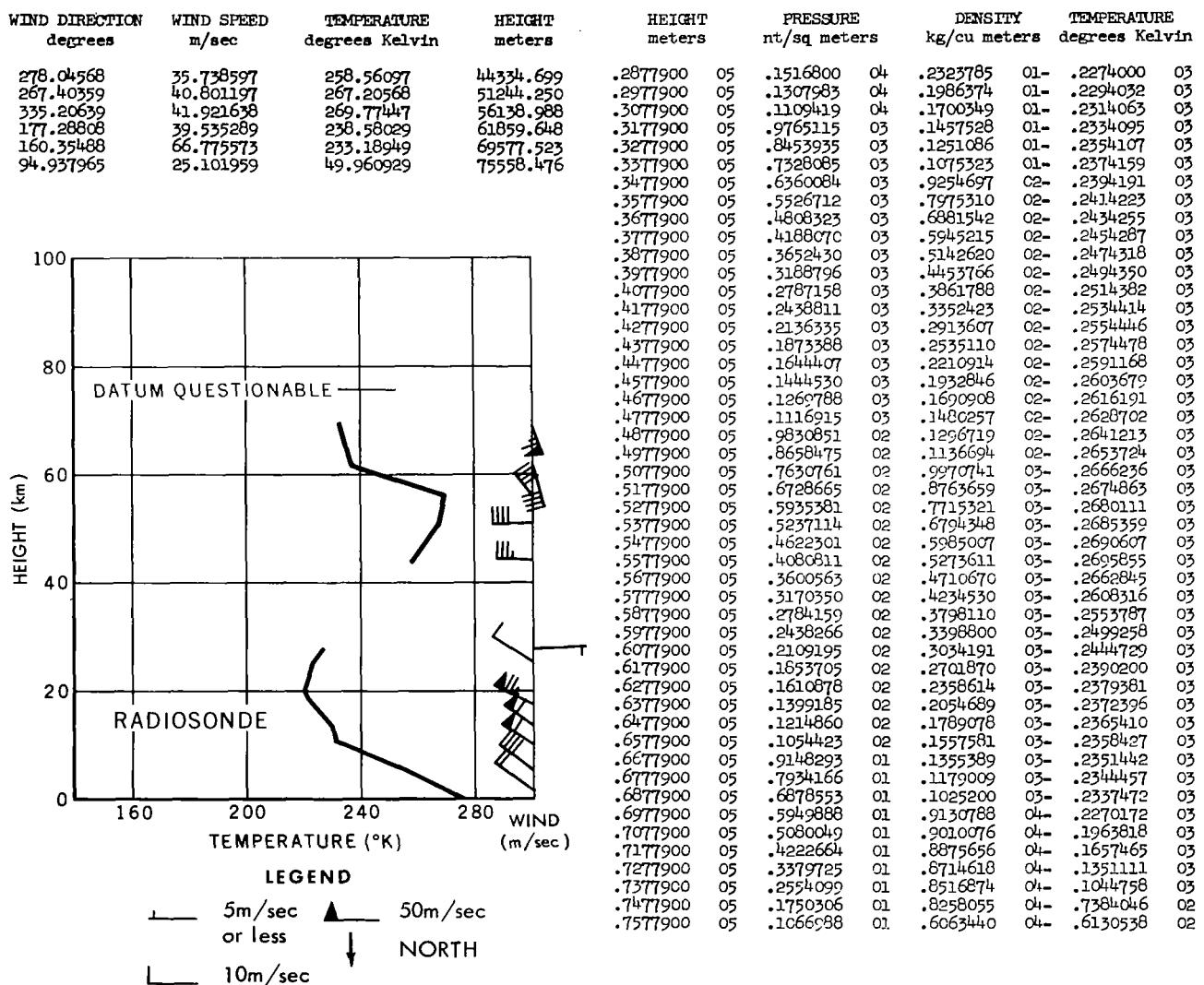


FIGURE 5
5 MAY 1961, 1800 EST, WALLOPS ISLAND, VA.

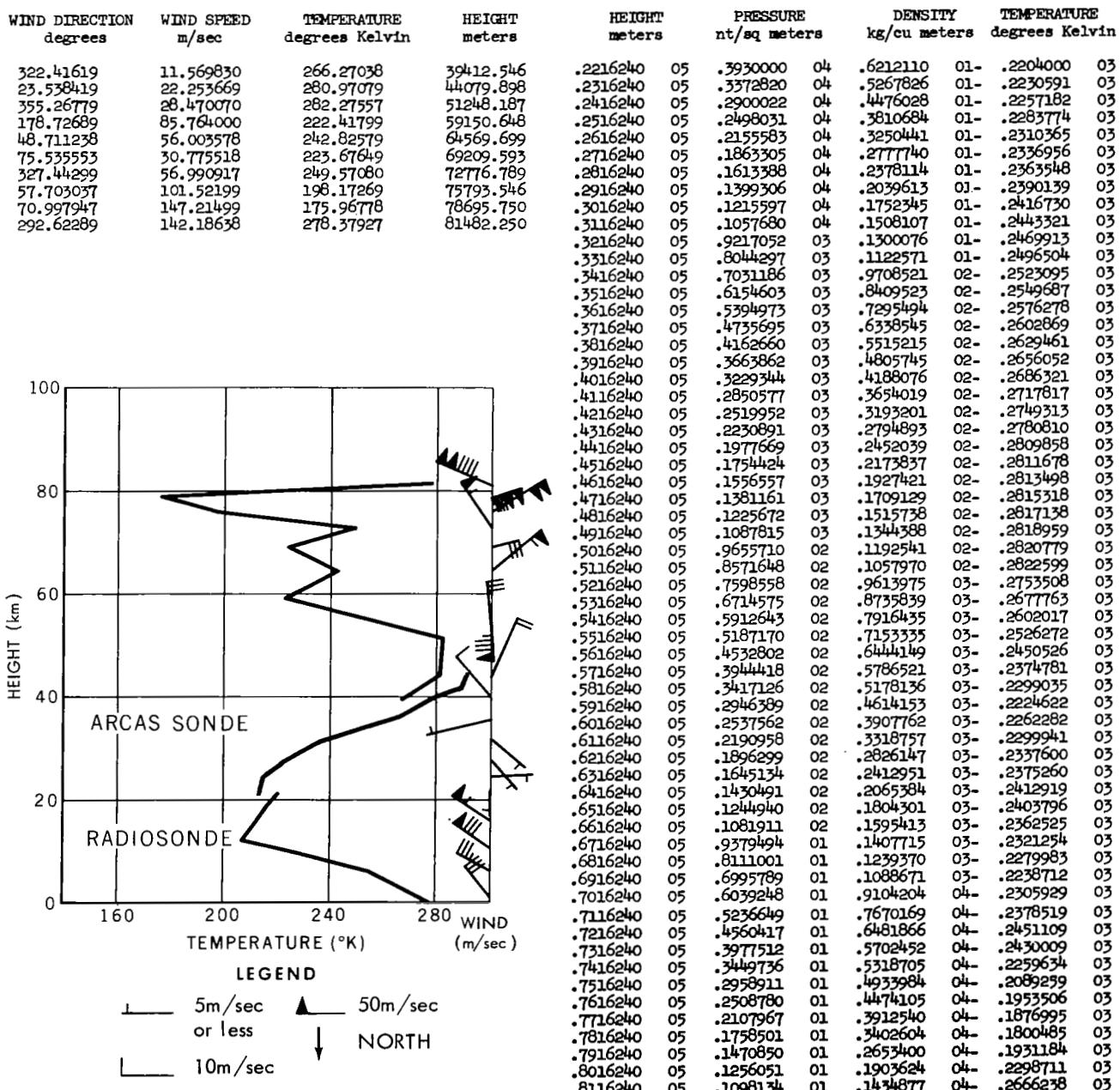


FIGURE 6
5 MAY 1961, 2354 EST, WALLOPS ISLAND, VA.

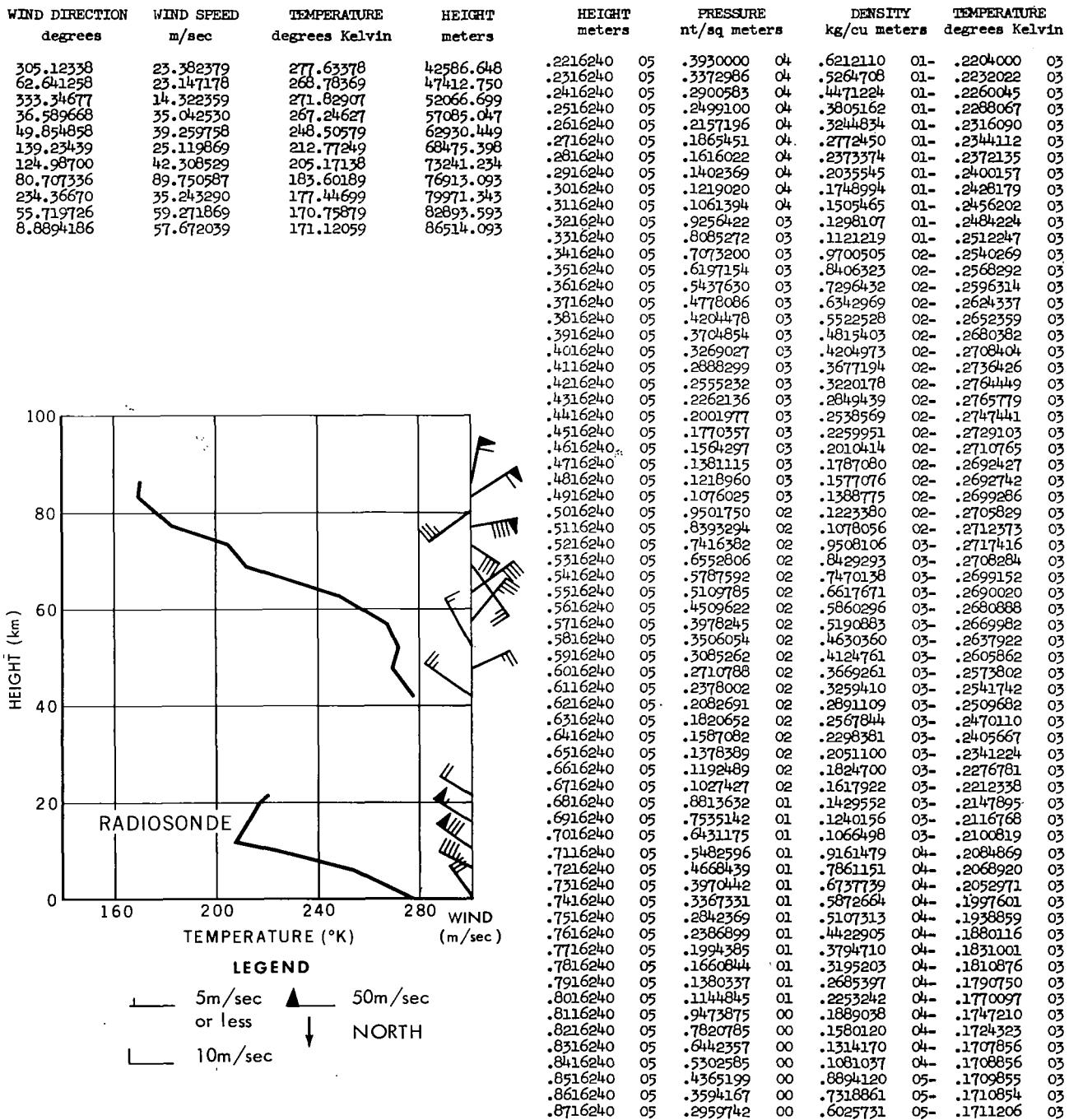


FIGURE 7
13 JULY 1961, 1707 EST, WALLOPS ISLAND, VA.

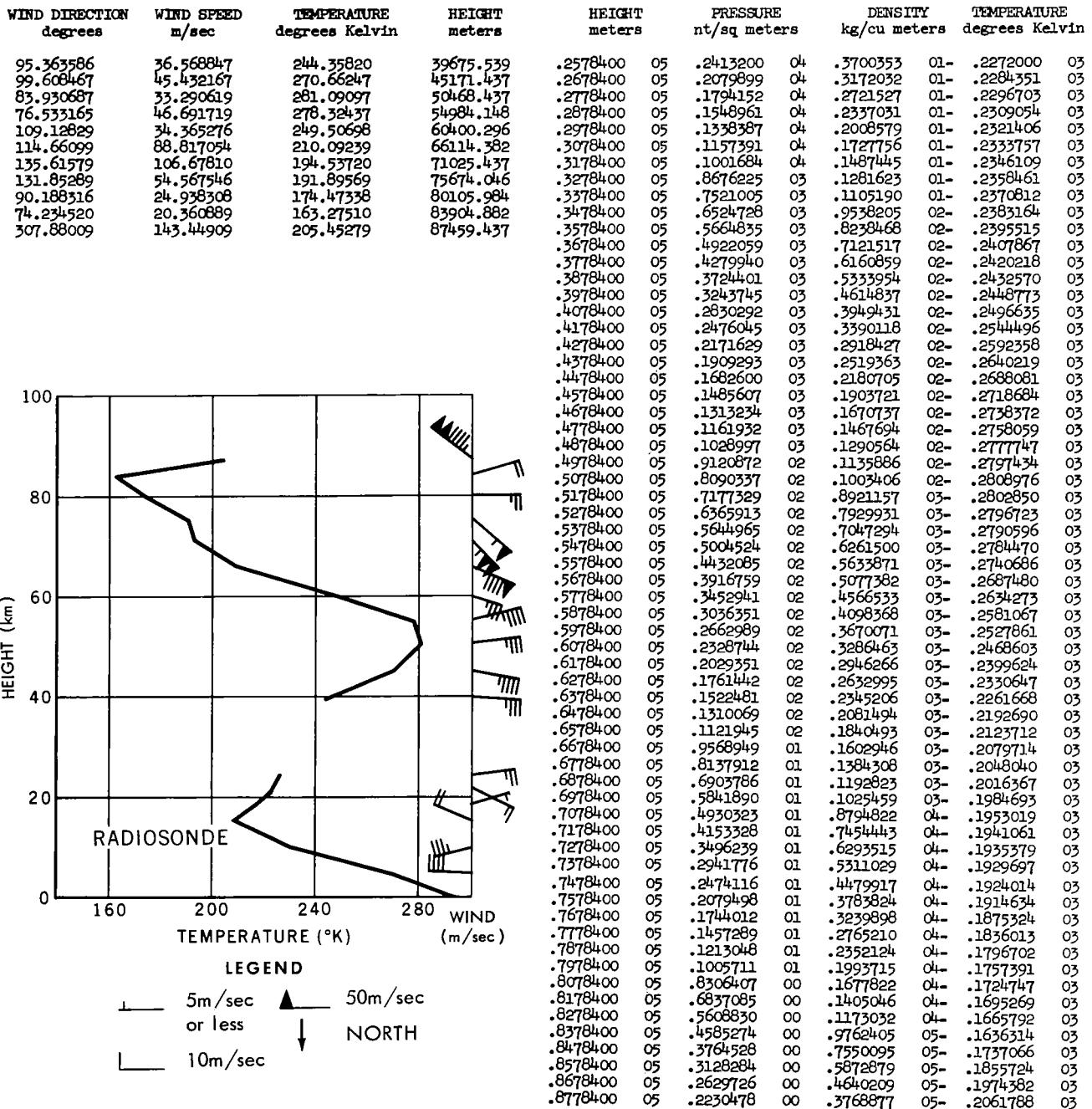


FIGURE 8
14 JULY 1961, 1102 EST, WALLOPS ISLAND, VA.

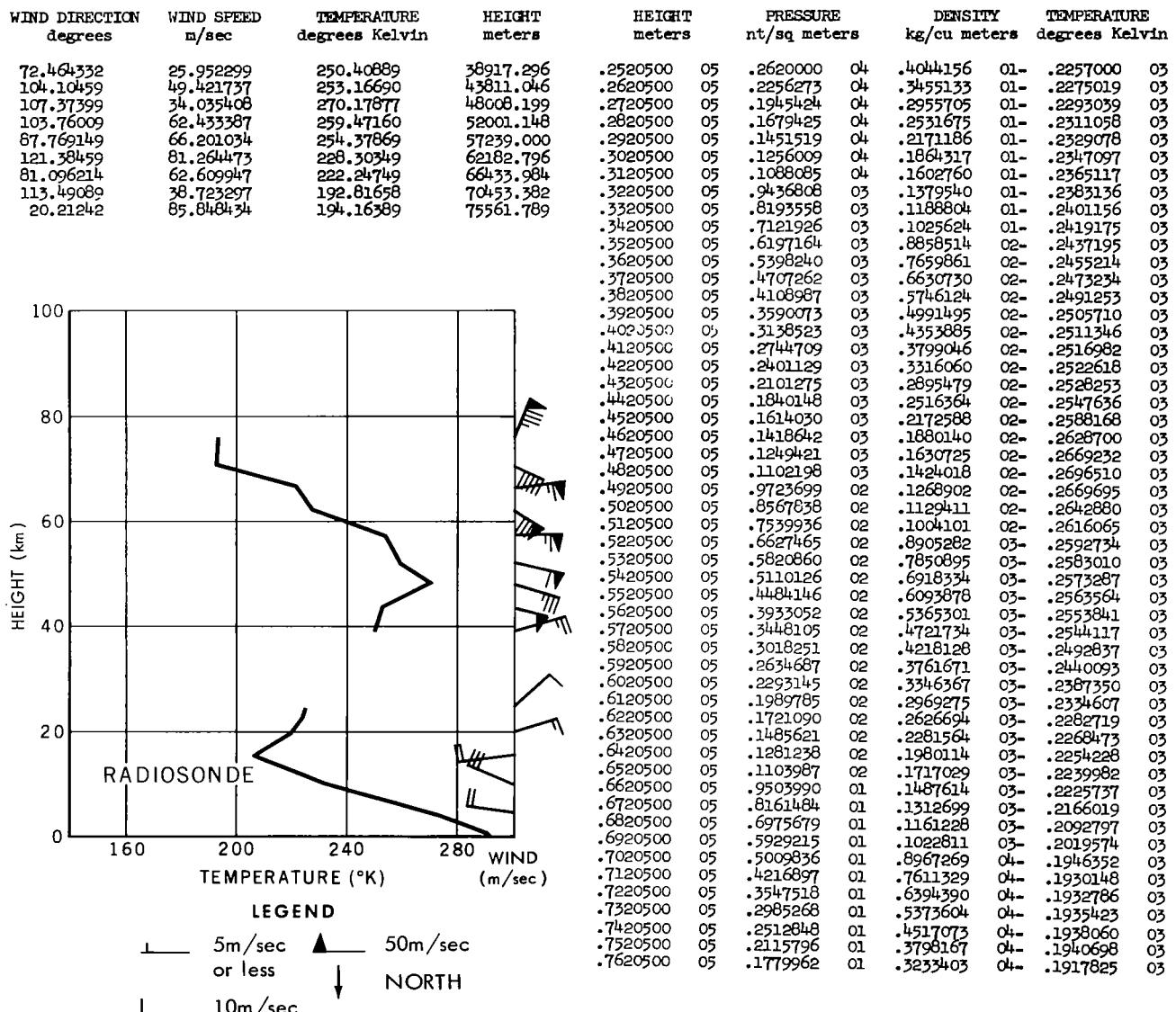


FIGURE 9
20 JULY 1961, 0530 EST, WALLOPS ISLAND, VA

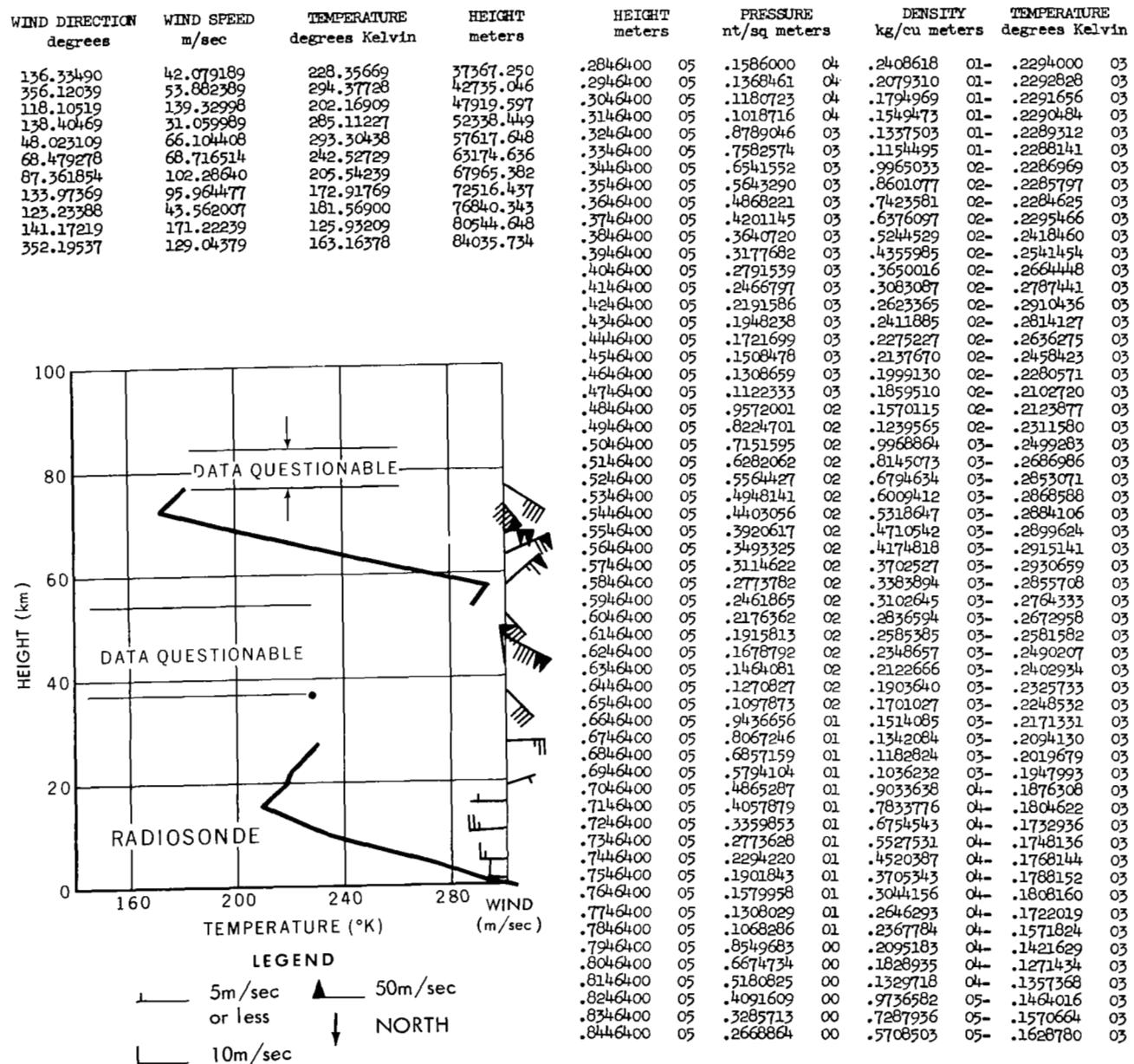


FIGURE 10
16 SEPTEMBER 1961, 1855 EST, WALLOPS ISLAND, VA.

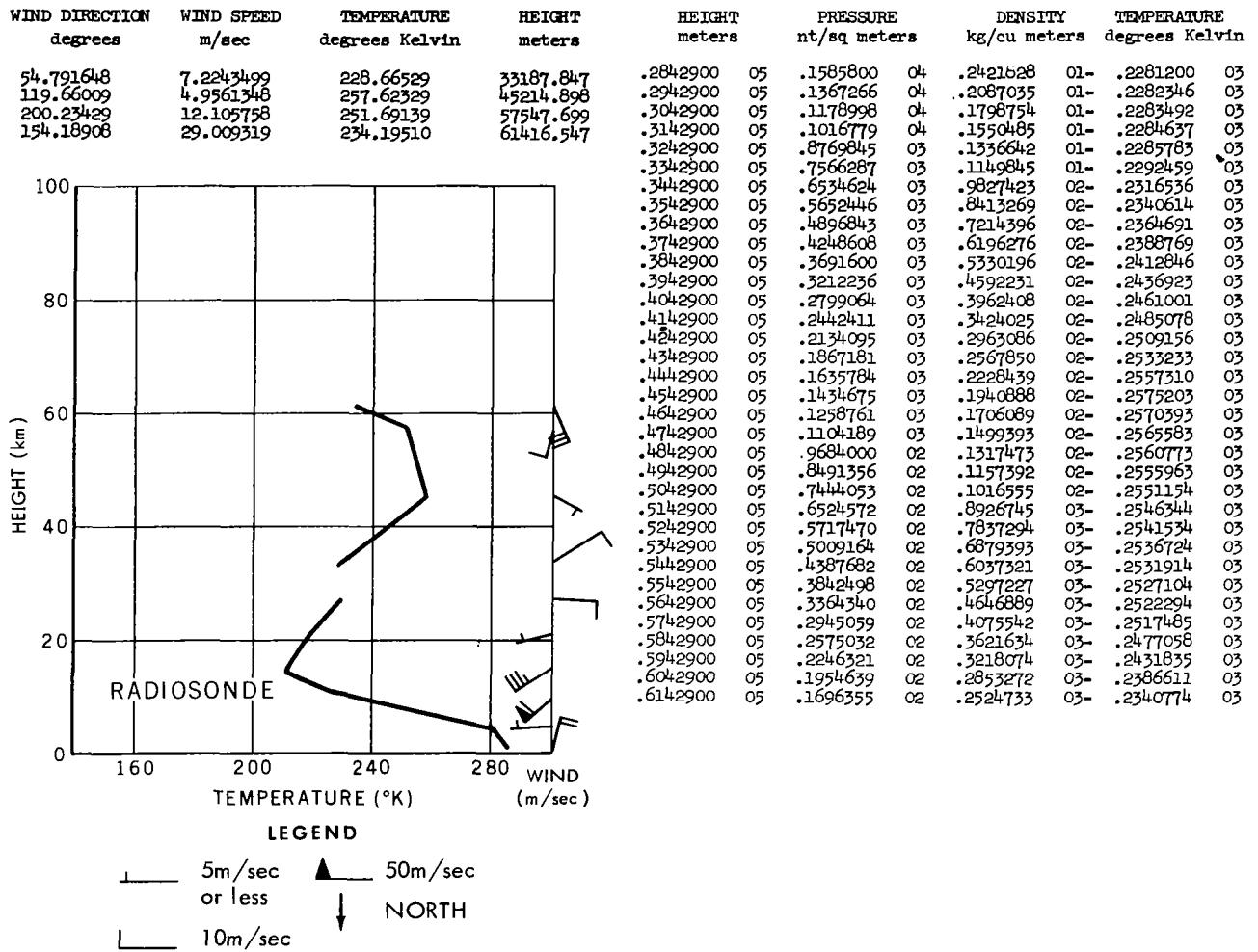


FIGURE 11
1 MARCH 1962, 1905 EST, WALLOPS ISLAND, VA

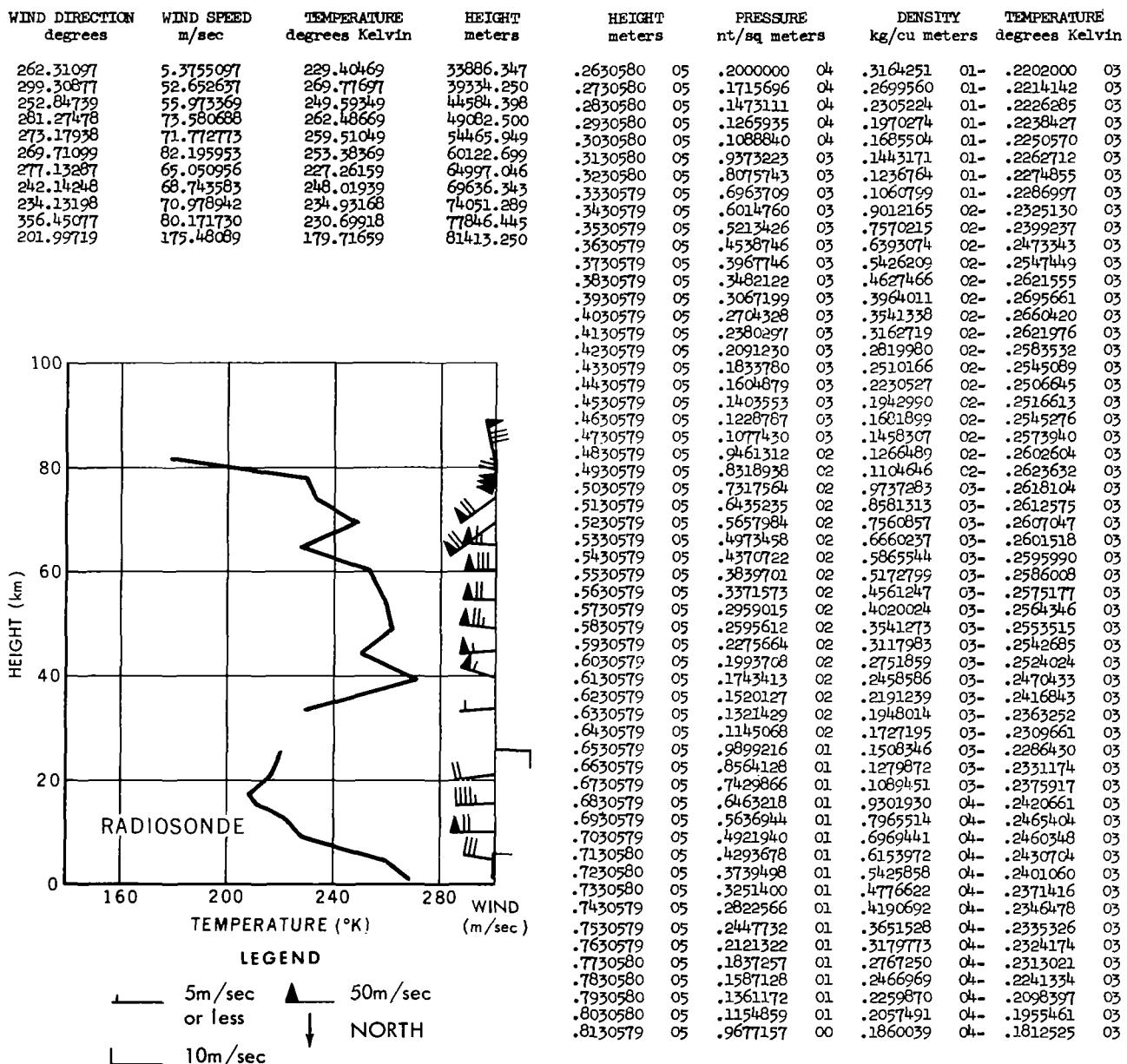


FIGURE 12
2 MARCH 1962, 0615 EST, WALLOPS ISLAND, VA.

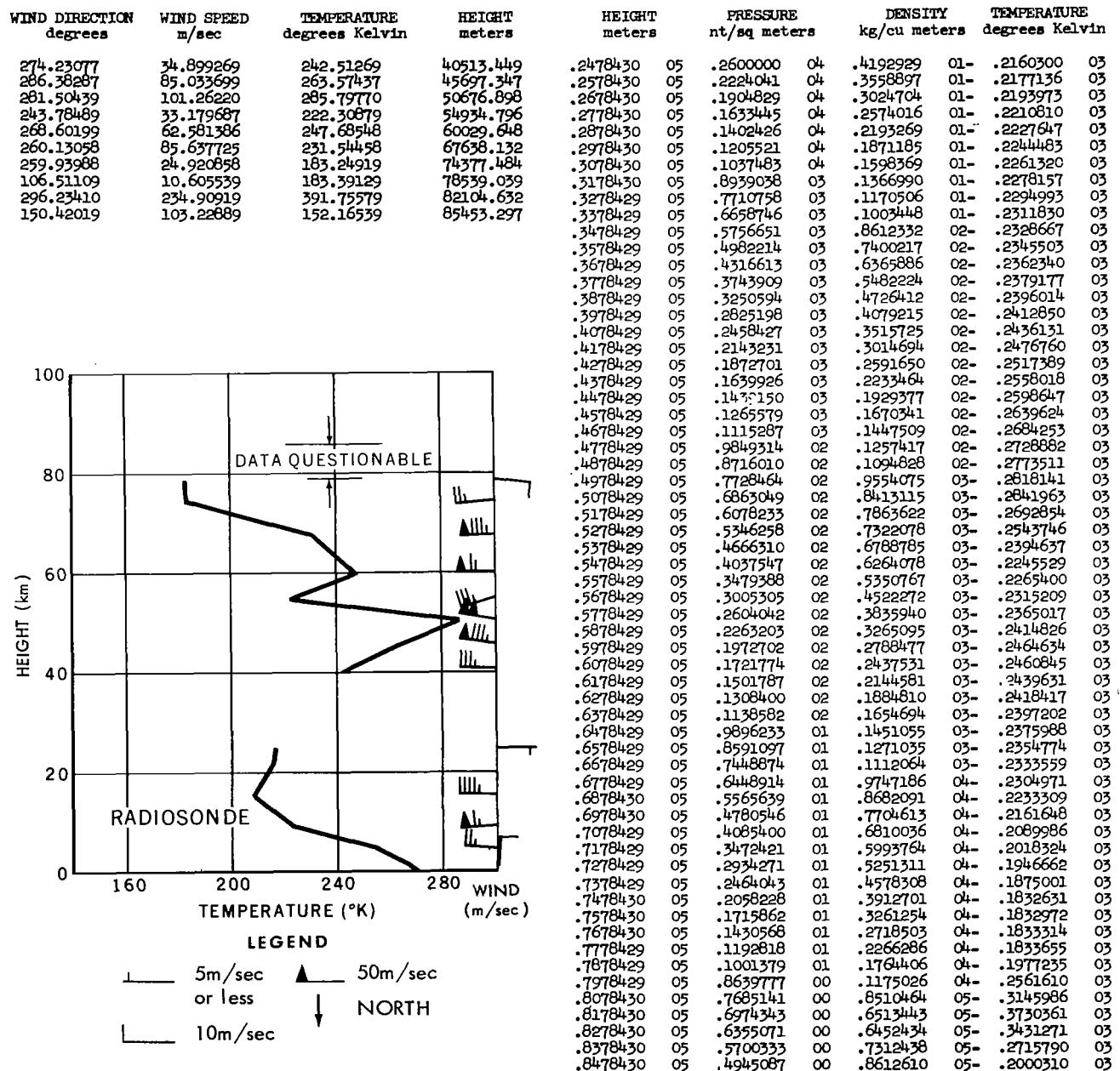


FIGURE 13
23 MARCH 1962, 1854 EST, WALLOPS ISLAND, VA.

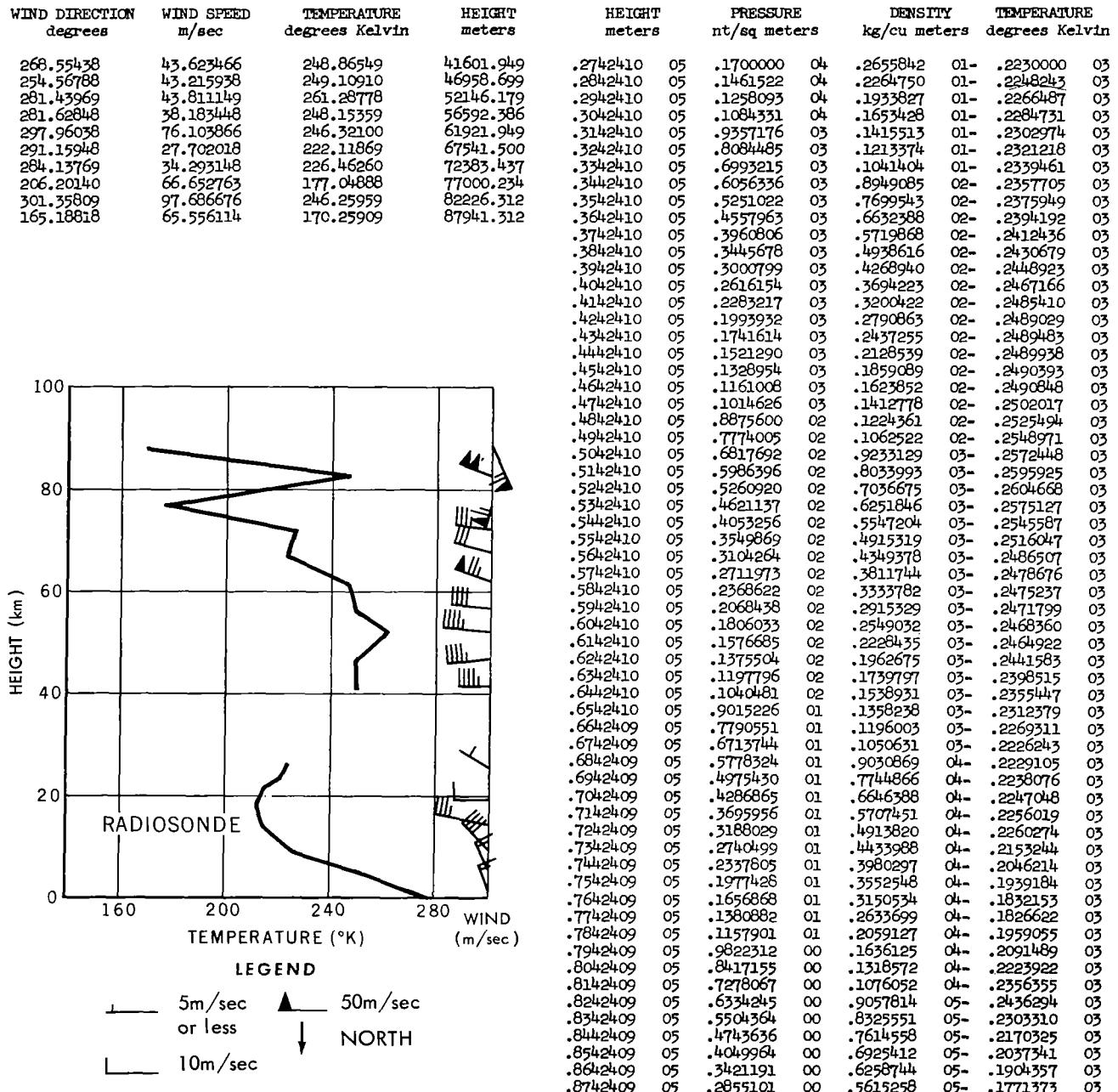


FIGURE 14

27 MARCH 1962, 1904 EST, WALLOPS ISLAND, VA.

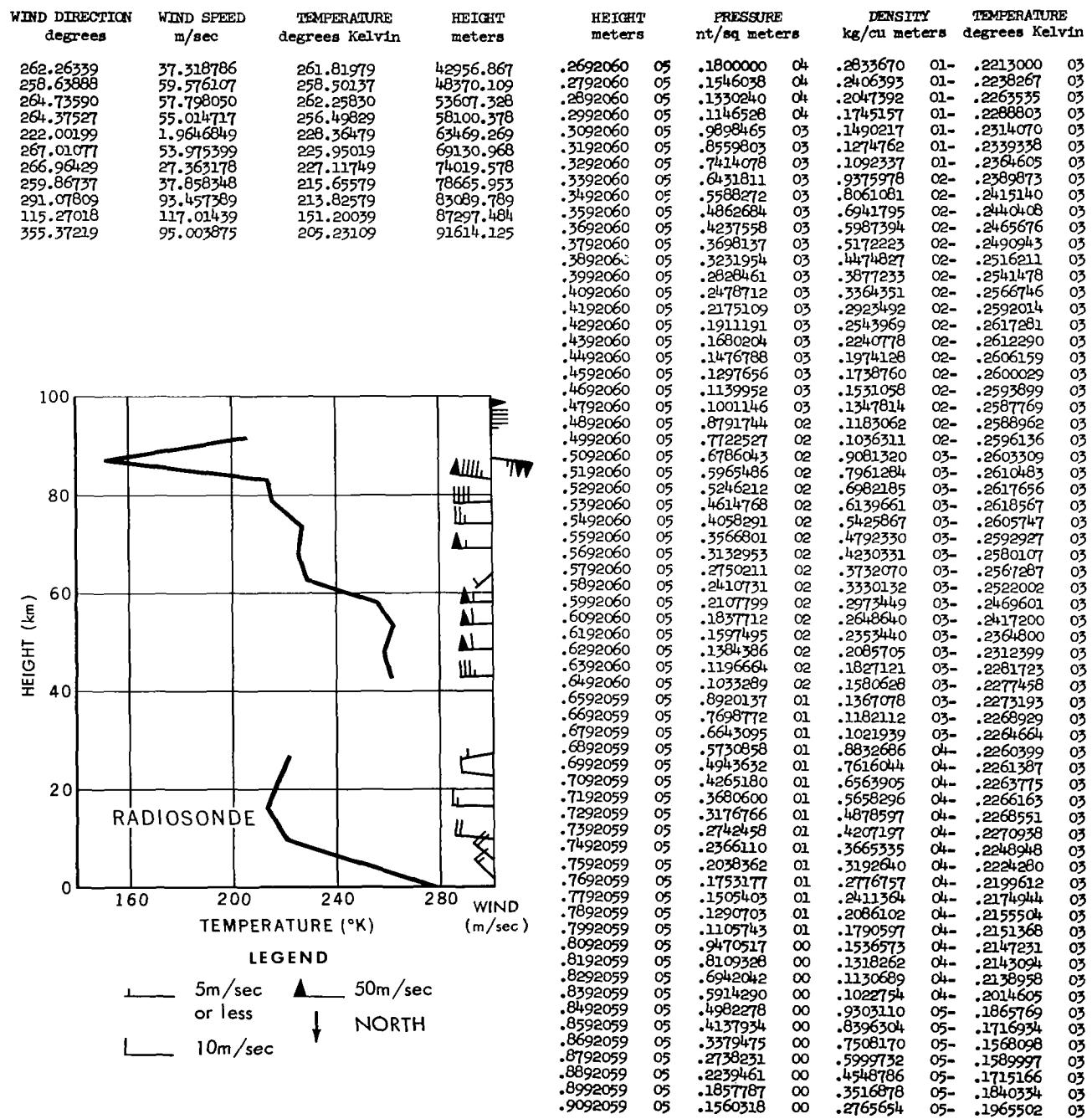


FIGURE 15
17 APRIL 1962, 0429 EST, WALLOPS ISLAND, VA.

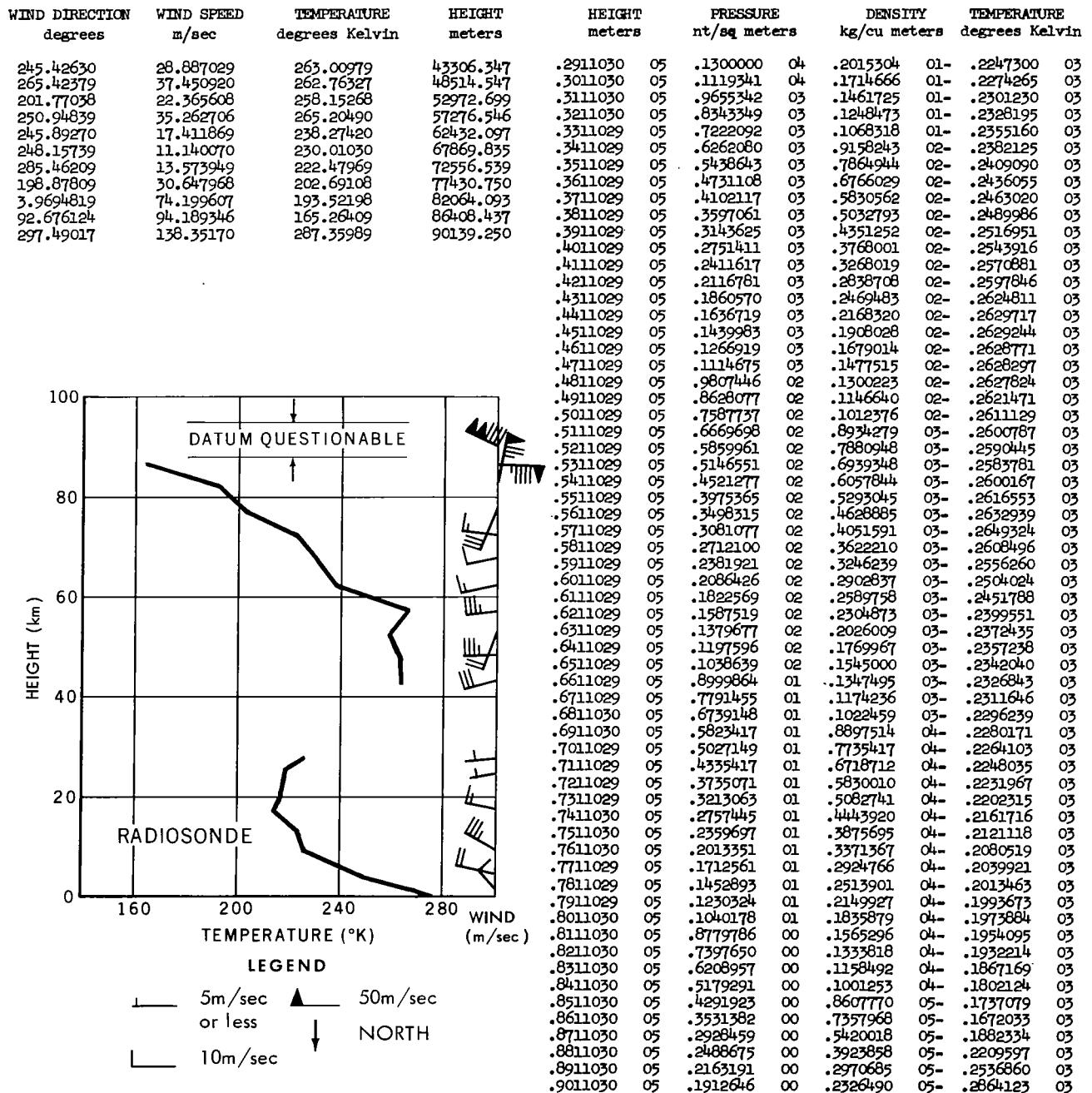


FIGURE 16
6 JUNE 1962, 2005 EST, WALLOPS ISLAND, VA.

WIND DIRECTION degrees	WIND SPEED m/sec	TEMPERATURE degrees Kelvin	HEIGHT meters	HEIGHT meters	PRESSURE nt/sq meters	DENSITY kg/cu meters	TEMPERATURE degrees Kelvin
100.23349	35.039177	271.12729	45967.500	.2782370	.05 .1700000	.04 .2561204	01- .2312400
112.12339	31.965488	265.44758	51428.398	.2882370	.05 .1469582	.01 .2193208	01- .2334384
85.151390	20.540390	268.92028	56624.398	.2982370	.05 .12712189	.04 .1880904	01- .2356368
76.249366	37.992378	241.96479	62684.597	.3082370	.05 .1102834	.04 .1615445	01- .2378352
86.465759	47.108570	208.31379	69435.039	.3182370	.05 .9573240	.03 .1389457	01- .2400336
102.19909	72.069656	197.25399	75832.382	.3282370	.05 .8321220	.03 .1196778	01- .2422320
100.33849	77.084068	168.90759	81279.049	.3382370	.05 .7242419	.03 .1032254	01- .2444304
219.76649	81.912193	174.49778	85927.898	.3482370	.05 .6311593	.03 .8915658	02- .2466288
5.6612997	193.16529	167.00509	89940.898	.3582370	.05 .5507353	.03 .7710869	02- .2488272
97.556236	223.62478	145.78129	93665.695	.3682370	.05 .4811559	.03 .6677687	02- .2510256
				.3782370	.05 .4208802	.03 .5790443	02- .2532240
				.3882370	.05 .3685967	.03 .5027148	02- .2554224
				.3982370	.05 .3231886	.03 .4370523	02- .2576207
				.4082370	.05 .2837027	.03 .3804088	02- .2598191
				.4182370	.05 .2493247	.03 .3315073	02- .2620175
				.4282370	.05 .2193578	.03 .2892359	02- .2642159
				.4382370	.05 .1932052	.03 .2526500	02- .2664143
				.4482370	.05 .1703549	.03 .2209460	02- .2686127
				.4582370	.05 .1503671	.03 .1934393	02- .2708111
				.4682370	.05 .1327794	.03 .1711766	02- .2702367
				.4782370	.05 .1172096	.03 .1516882	02- .2691966
				.4882370	.05 .1034197	.03 .1343609	02- .2681565
				.4982370	.05 .9121133	.02 .1189615	02- .2671164
				.5082370	.05 .8040792	.02 .1052812	02- .2660763
				.5182370	.05 .7086315	.02 .9291121	03- .2657116
				.5282370	.05 .6245859	.02 .8168621	03- .2663800
				.5382370	.05 .5507040	.02 .7184533	03- .2670483
				.5482370	.05 .4857337	.02 .6320927	03- .2677168
				.5582370	.05 .4285786	.02 .5563270	03- .2683852
				.5682370	.05 .3781911	.02 .4911563	03- .2680339
				.5782370	.05 .3333633	.02 .4406094	03- .2635859
				.5882370	.05 .2952304	.02 .3942177	03- .2591379
				.5982370	.05 .2573672	.02 .3520461	03- .2546900
				.6082370	.05 .2253809	.02 .3137727	03- .2502420
				.6182370	.05 .1969090	.02 .2790953	03- .2457940
				.6282370	.05 .1716138	.02 .2478020	03- .2412713
				.6382370	.05 .1491656	.02 .2199319	.03- .2362863
				.6482370	.05 .1292725	.02 .1947090	.03- .2313013
				.6582369	.05 .1116886	.02 .1719297	.03- .2263163
				.6682369	.05 .9618718	.01 .1514023	.03- .2213313
				.6782369	.05 .7255966	.01 .1329464	.03- .2163463
				.6882369	.05 .7061436	.01 .1163927	.03- .2113613
				.6982369	.05 .6020476	.01 .1010123	.03- .2076419
				.7082369	.05 .5122469	.01 .8666698	.04- .2059131
				.7182369	.05 .4352695	.01 .7426672	.04- .2041842
				.7282369	.05 .3693669	.01 .6355604	.04- .2024554
				.7382369	.05 .3130174	.01 .5432774	.04- .2007266
				.7482369	.05 .2614897	.01 .4637561	.04- .1989978
				.7582369	.05 .2238624	.01 .3953489	.04- .1972690
				.7682369	.05 .1886279	.01 .3420963	.04- .1920948
				.7782369	.05 .1582039	.01 .2949091	.04- .1868905
				.7882369	.05 .1320369	.01 .2531813	.04- .1816861
				.7982369	.05 .1096266	.01 .2164066	.04- .1764818
				.8082369	.05 .9052001	.00 .1841207	.04- .1712774
				.8182369	.05 .7445886	.00 .1529835	.04- .1695625
				.8282369	.05 .6123329	.00 .1249243	.04- .1707650
				.8382369	.05 .5042907	.00 .1021628	.04- .1719675
				.8482369	.05 .4158986	.00 .8367063	.05- .1731700
				.8582369	.05 .3434779	.00 .6662448	.05- .1743725
				.8682369	.05 .2836304	.00 .5717470	.05- .1728252
				.8782369	.05 .2337798	.00 .4764040	.05- .1709581
				.8882369	.05 .1922939	.00 .3961897	.05- .1690910
				.8982369	.05 .1578369	.00 .3288277	.05- .1672239
				.9082369	.05 .1290085	.00 .2774782	.05- .1619749
				.9182369	.05 .1047229	.00 .2334559	.05- .1562769
				.9282369	.05 .8435857	.01- .1951745	.05- .1505790
				.9382369	.05 .6706524	.01- .1684508	.05- .1387020

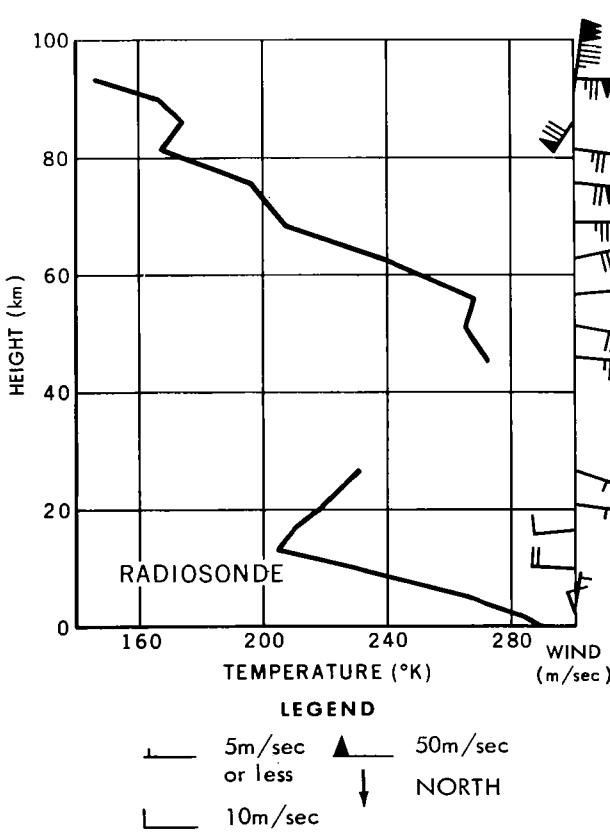


FIGURE 17
7 JUNE 1962, 2053 EST, WALLOPS ISLAND, VA.

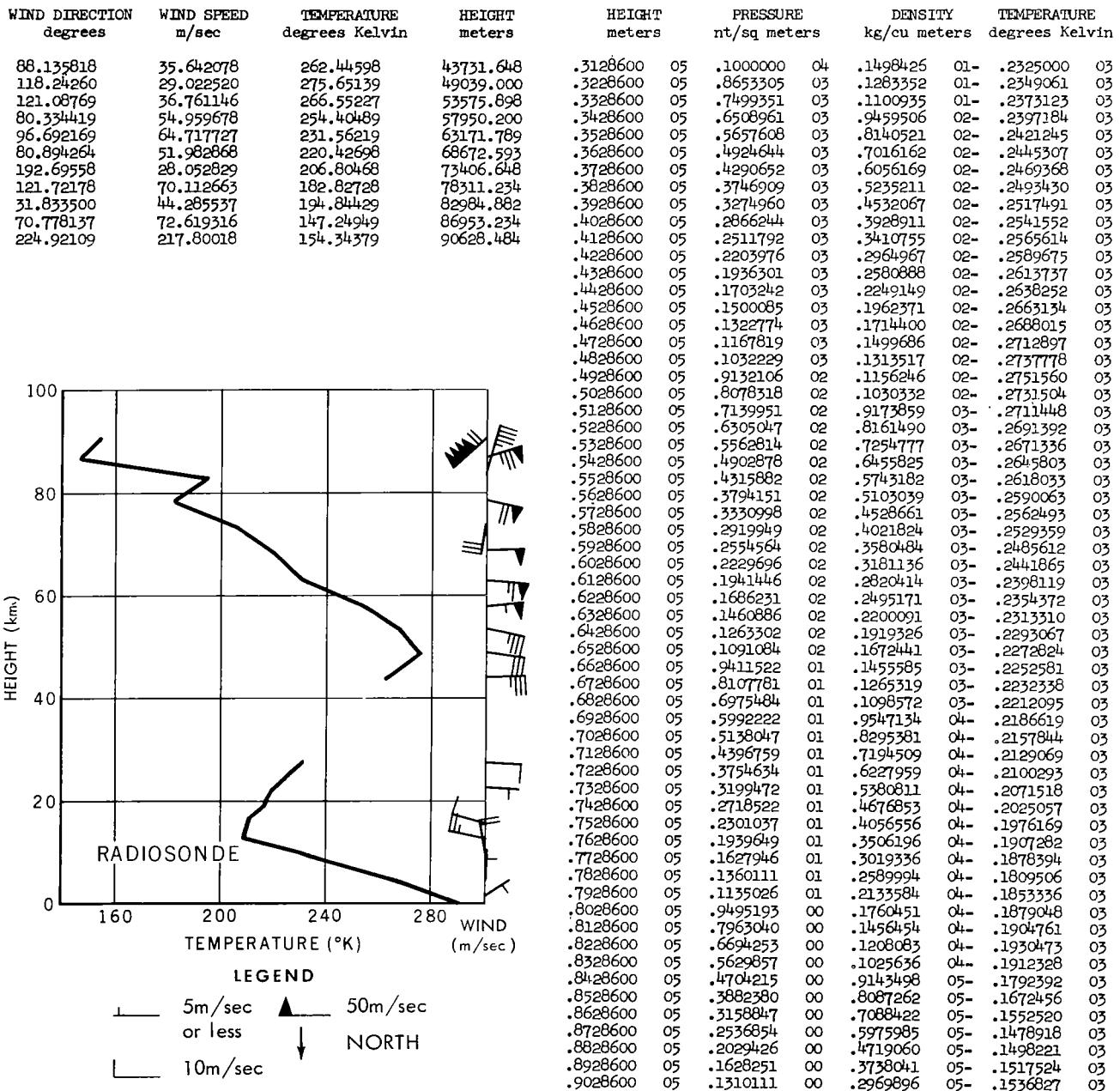


FIGURE 18
1 DECEMBER 1962, 1625 EST, WALLOPS ISLAND, VA.

WIND DIRECTION degrees	WIND SPEED m/sec	TEMPERATURE degrees Kelvin	HEIGHT meters	HEIGHT meters	PRESSURE nt/sq meters	DENSITY kg/cu meters	TEMPERATURE degrees Kelvin
273.83029	53.767238	245.67549	40618.347	.2889260	05 .1300000	04 .2061350	01-.2197100 .03
267.66479	83.497436	259.56347	46206.437	.2989260	05 .1115347	04 .1750907	01-.2219244 .03
265.29300	94.068039	256.97729	50987.546	.3089260	05 .9584243	03 .1489701	01-.2241388 .03
283.99978	99.636158	255.52859	55623.097	.3189260	05 .8248469	03 .1269556	01-.2265532 .03
276.75988	85.044586	241.85888	61199.898	.3289260	05 .7109576	03 .1083645	01-.2285676 .03
295.78497	80.256599	230.72470	67064.695	.3389260	05 .6136999	03 .9264295	02-.2307820 .03
216.34069	36.389019	216.65219	72110.546	.3489260	05 .5305159	03 .7932451	02-.2329964 .03
203.29139	115.02049	188.27578	77416.687	.3589260	05 .4592600	03 .6802359	02-.2352108 .03
329.80078	196.25229	239.28830	82479.836	.3689260	05 .3981302	03 .5841933	02-.2374252 .03
46.157417	45.832988	179.11309	86794.796	.3789260	05 .3456103	03 .5024425	02-.2396396 .03
346.41769	389.29647	271.31540	90863.945	.3889260	05 .3004224	03 .4327502	02-.2418540 .03
				.3989260	05 .2614878	03 .3732486	02-.240684 .03
				.4089260	05 .2278992	03 .3222819	02-.2463571 .03
				.4189260	05 .1988968	03 .2784593	02-.2488423 .03
				.4289260	05 .1738276	03 .2409554	02-.2513276 .03
				.4389260	05 .1521260	03 .2088084	02-.2538129 .03
				.4489260	05 .1333123	03 .1812104	02-.2562982 .03
				.4589260	05 .1169791	03 .1574816	02-.2587835 .03
				.4689260	05 .1027264	03 .1380759	02-.2591923 .03
				.4789260	05 .9021051	02 .1215068	02-.2586514 .03
				.4889260	05 .7920117	02 .1069016	02-.2581105 .03
				.4989260	05 .6951930	02 .9403056	03-.2575695 .03
				.5089260	05 .6100673	02 .8269028	03-.2570286 .03
				.5189260	05 .5352674	02 .7264614	03-.2566944 .03
				.5289260	05 .4695803	02 .6380881	03-.2563819 .03
				.5389260	05 .4119050	02 .5603992	03-.2560694 .03
				.5489260	05 .3612704	02 .4921112	03-.2557569 .03
				.5589260	05 .3167762	02 .4330075	03-.2540680 .03
				.5689260	05 .2775331	02 .3830493	03-.2524168 .03
				.5789260	05 .2426479	02 .3384638	03-.2499656 .03
				.5889260	05 .2122270	02 .2987159	03-.2475145 .03
				.5989260	05 .1852264	02 .2633194	03-.2450633 .03
				.6089260	05 .1614469	02 .2318330	03-.2426121 .03
				.6189260	05 .1405455	02 .2035546	03-.2405438 .03
				.6289260	05 .1222150	02 .1784144	03-.2386453 .03
				.6389260	05 .1061614	02 .1562215	03-.2367468 .03
				.6489260	05 .9211609	01 .1366489	03-.2348484 .03
				.6589259	05 .7984050	01 .1194040	03-.2329499 .03
				.6689259	05 .6912293	01 .1042249	03-.2310514 .03
				.6789259	05 .5976166	01 .9114961	04-.2284157 .03
				.6889259	05 .5158077	01 .7964442	04-.2256268 .03
				.6989259	05 .4444041	01 .6947799	04-.2228379 .03
				.7089259	05 .3821849	01 .6050795	04-.2200490 .03
				.7189259	05 .3280607	01 .5260566	04-.2172600 .03
				.7289259	05 .2808563	01 .4605162	04-.2124699 .03
				.7389259	05 .2595546	01 .4029562	04-.2071221 .03
				.7489259	05 .2034884	01 .3513436	04-.2017742 .03
				.7589259	05 .1721051	01 .3052474	04-.1964264 .03
				.7689259	05 .1448981	01 .2641856	04-.1910785 .03
				.7789259	05 .1218167	01 .2198107	04-.1930707 .03
				.7889259	05 .1029564	01 .1765646	04-.2031459 .03
				.7989259	05 .8773210	00 .1433463	04-.2132211 .03
				.8089259	05 .7551704	00 .1175086	04-.2232964 .03
				.8189259	05 .6509872	00 .9718126	05-.2333717 .03
				.8289259	05 .5645094	00 .8421372	05-.2335321 .03
				.8389259	05 .4873984	00 .7732802	05-.2195864 .03
				.8489259	05 .4168033	00 .7061230	05-.2056407 .03
				.8589259	05 .3525550	00 .6407291	05-.1916949 .03
				.8689259	05 .2949986	00 .5667752	05-.1813290 .03
				.8789259	05 .2482211	00 .4239283	05-.2030879 .03
				.8889259	05 .2127682	00 .3269587	05-.2266468 .03
				.8989259	05 .1849879	00 .2585053	05-.2493057 .03
				.9089259	05 .1628287	00 .2090840	05-.2713116 .03

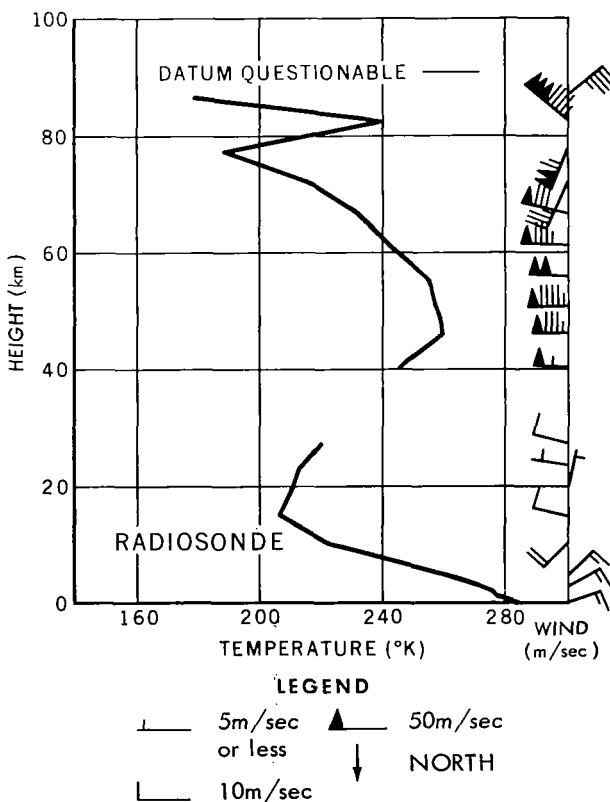


FIGURE 19
4 DECEMBER 1962, 0105 CST FT. CHURCHILL

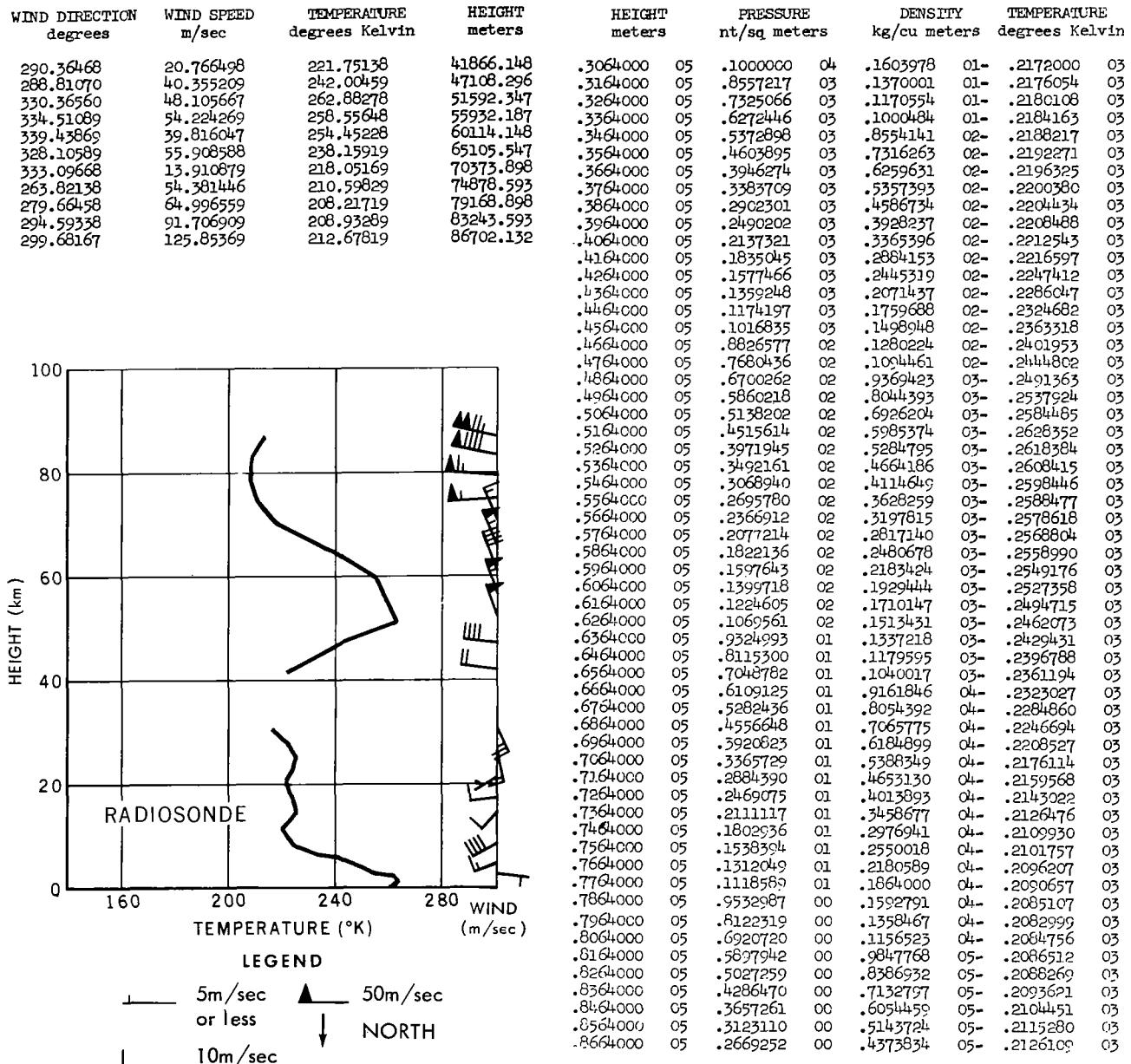


FIGURE 20
6 DECEMBER 1962, 0032 EST, WALLOPS ISLAND, VA.

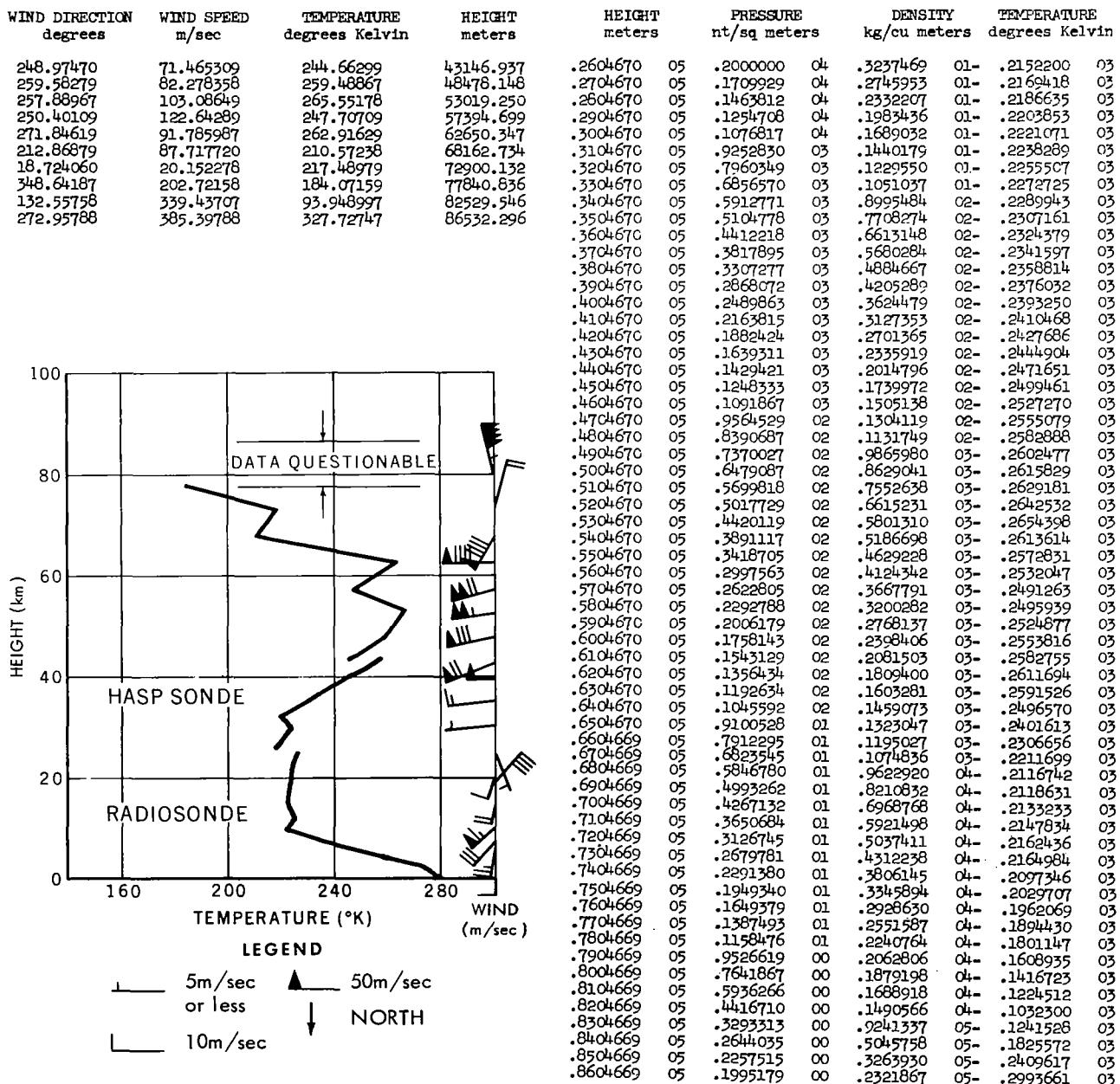


FIGURE 21
5 DECEMBER 1962, 2343 CST FT. CHURCHILL

WIND DIRECTION degrees	WIND SPEED m/sec	TEMPERATURE degrees Kelvin	HEIGHT meters	HEIGHT meters	PRESSURE nt/sq meters	DENSITY kg/cu meters	TEMPERATURE degrees Kelvin
284.19079	32.374157	222.58299	41977.500	.2760000 05	.1300000 04	.2085171 01-	.2172000 03
271.21618	29.083198	240.94349	47418.187	.2860000 05	.1112262 04	.1780973 01-	.2175744 03
502.20727	56.672359	250.83938	52084.347	.2960000 05	.9519342 03	.1521635 01-	.2179488 03
311.63467	21.642078	262.77108	56597.250	.3060000 05	.8149743 03	.1300476 01-	.2183232 03
302.11697	3.6421175	261.85049	60956.847	.3160000 05	.6979395 03	.1111814 01-	.2186976 03
55.247146	20.369548	238.49319	66180.343	.3260000 05	.5979000 03	.9506234 02-	.2190720 03
127.13758	42.825447	220.66958	71686.445	.3360000 05	.5123596 03	.8134008 02-	.2194464 03
235.76329	15.062839	209.03039	76435.188	.3460000 05	.4391932 03	.6960573 02-	.2198208 03
257.03728	34.519538	187.90699	80973.046	.3560000 05	.3765916 03	.5958280 02-	.2201952 03
300.67657	119.71708	208.01059	85273.843	.3660000 05	.3230128 03	.5101904 02-	.2205696 03
301.21899	88.249855	198.10629	88936.548	.3760000 05	.2771425 03	.4369975 02-	.2209440 03
			.3860000 05	.2370595 03	.37414217 02-	.2213181 03	
			.3960000 05	.2042064 03	.3209046 02-	.2216928 03	
			.4060000 05	.1753683 03	.2751216 02-	.2220672 03	
			.4160000 05	.1506487 03	.2359432 02-	.2224416 03	
			.4260000 05	.1295342 03	.2008496 02-	.2246837 03	
			.4360000 05	.1115930 03	.1704704 02-	.2260564 03	
			.4460000 05	.9635183 02	.1450417 02-	.2314330 03	
			.4560000 05	.8337108 02	.1237006 02-	.2348077 03	
			.4660000 05	.7229470 02	.1057441 02-	.2381824 03	
			.4760000 05	.6281316 02	.9067743 03-	.2413291 03	
			.4860000 05	.5466005 02	.7822130 03-	.2434498 03	
			.4960000 05	.4762602 02	.6756566 03-	.2455706 03	
			.5060000 05	.4154754 02	.5813763 03-	.2476914 03	
			.5160000 05	.3628858 02	.5060746 03-	.2498122 03	
			.5260000 05	.3173518 02	.4383786 03-	.2522027 03	
			.5360000 05	.2779123 02	.3759156 03-	.2548466 03	
			.5460000 05	.2437178 02	.3297495 03-	.2574905 03	
			.5560000 05	.2142620 02	.2866334 03-	.2601344 03	
			.5660000 05	.1882057 02	.2495252 03-	.2627705 03	
			.5760000 05	.1656052 02	.2197378 03-	.2625593 03	
			.5860000 05	.1457086 02	.1934930 03-	.2623482 03	
			.5960000 05	.1281497 02	.1703727 03-	.2621370 03	
			.6060000 05	.1127792 02	.1500061 03-	.2619258 03	
			.6160000 05	.9914414 01	.1333731 03-	.2589746 03	
			.6260000 05	.8699873 01	.1190908 03-	.2545030 03	
			.6360000 05	.7616766 01	.1061290 03-	.2500314 03	
			.6460000 05	.6652800 01	.9438551 04-	.2455598 03	
			.6560000 05	.5796647 01	.8376431 04-	.2410882 03	
			.6660000 05	.5038653 01	.7402469 04-	.2371352 03	
			.6760000 05	.4370616 01	.650984 04-	.2338993 03	
			.6860000 05	.3763815 01	.5714909 04-	.2306634 03	
			.6960000 05	.3269279 01	.5008033 04-	.2274275 03	
			.7060000 05	.2818931 01	.4380495 04-	.2241517 03	
			.7160000 05	.2425500 01	.3824520 04-	.2209558 03	
			.7260000 05	.2082973 01	.3322162 04-	.2184344 03	
			.7360000 05	.1785787 01	.2680511 04-	.2159823 03	
			.7460000 05	.1528386 01	.2493629 04-	.2135303 03	
			.7560000 05	.1305801 01	.2155221 04-	.2110762 03	
			.7660000 05	.1113483 01	.1862643 04-	.2082630 03	
			.7760000 05	.9467931 00	.1620010 04-	.2036081 03	
			.7860000 05	.8020812 00	.1404517 04-	.1989532 03	
			.7960000 05	.6768652 00	.1213644 04-	.1942984 03	
			.8060000 05	.5688791 00	.1045058 04-	.1896435 03	
			.8160000 05	.4773957 00	.8715107 05-	.1908376 03	
			.8260000 05	.4017105 00	.7158104 05-	.1955100 03	
			.8360000 05	.3394235 00	.5906981 05-	.2001864 03	
			.8460000 05	.2879266 00	.4896448 05-	.2048608 03	
			.8560000 05	.2449343 00	.4119720 05-	.2071286 03	
			.8660000 05	.2083360 00	.3550499 05-	.2044246 03	
			.8760000 05	.1768338 00	.3054029 05-	.2017206 03	
			.8860000 05	.1497709 00	.2621780 05-	.1990166 03	

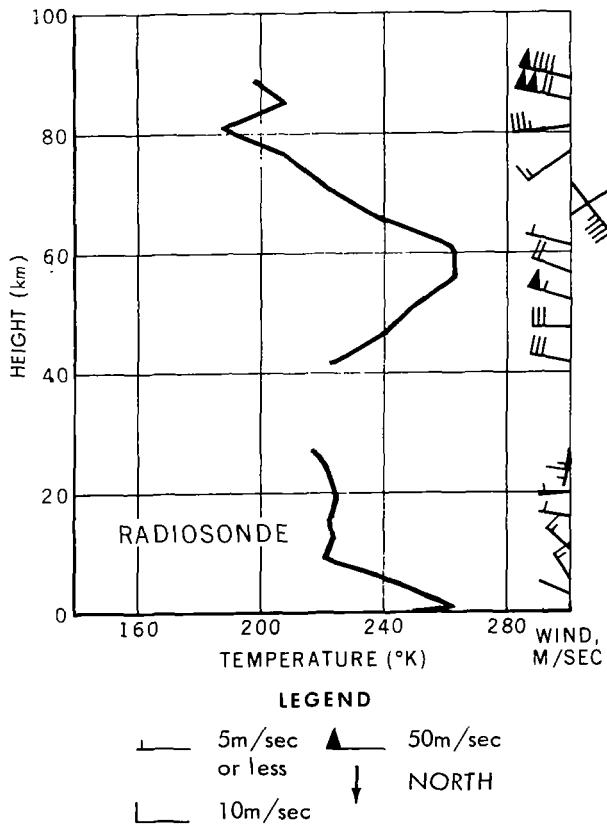


FIGURE 22
20 FEBRUARY 1963, 1734 CST FT. CHURCHILL

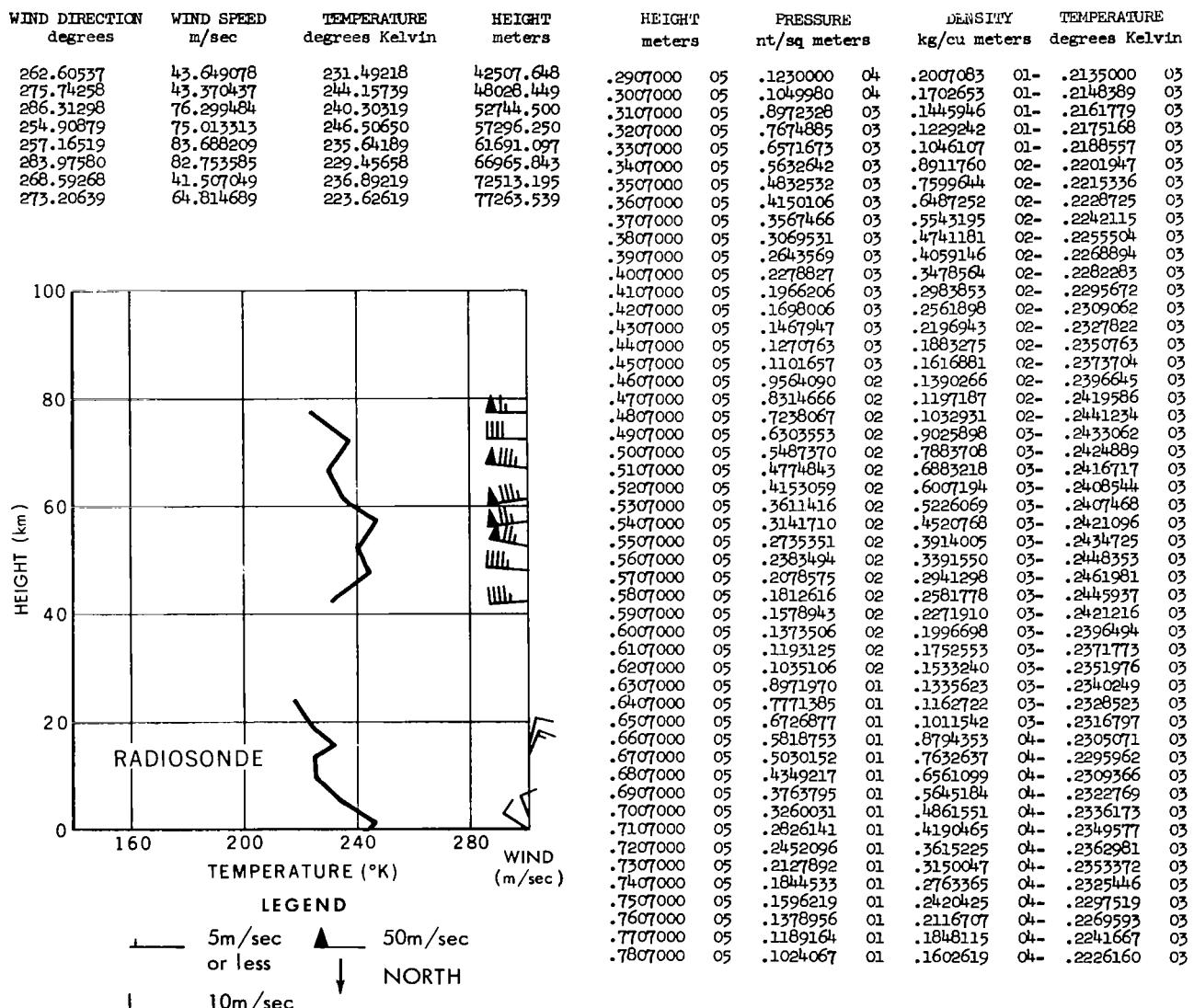


FIGURE 23
20 FEBRUARY 1963, 1847 EST, WALLOPS ISLAND, VA.

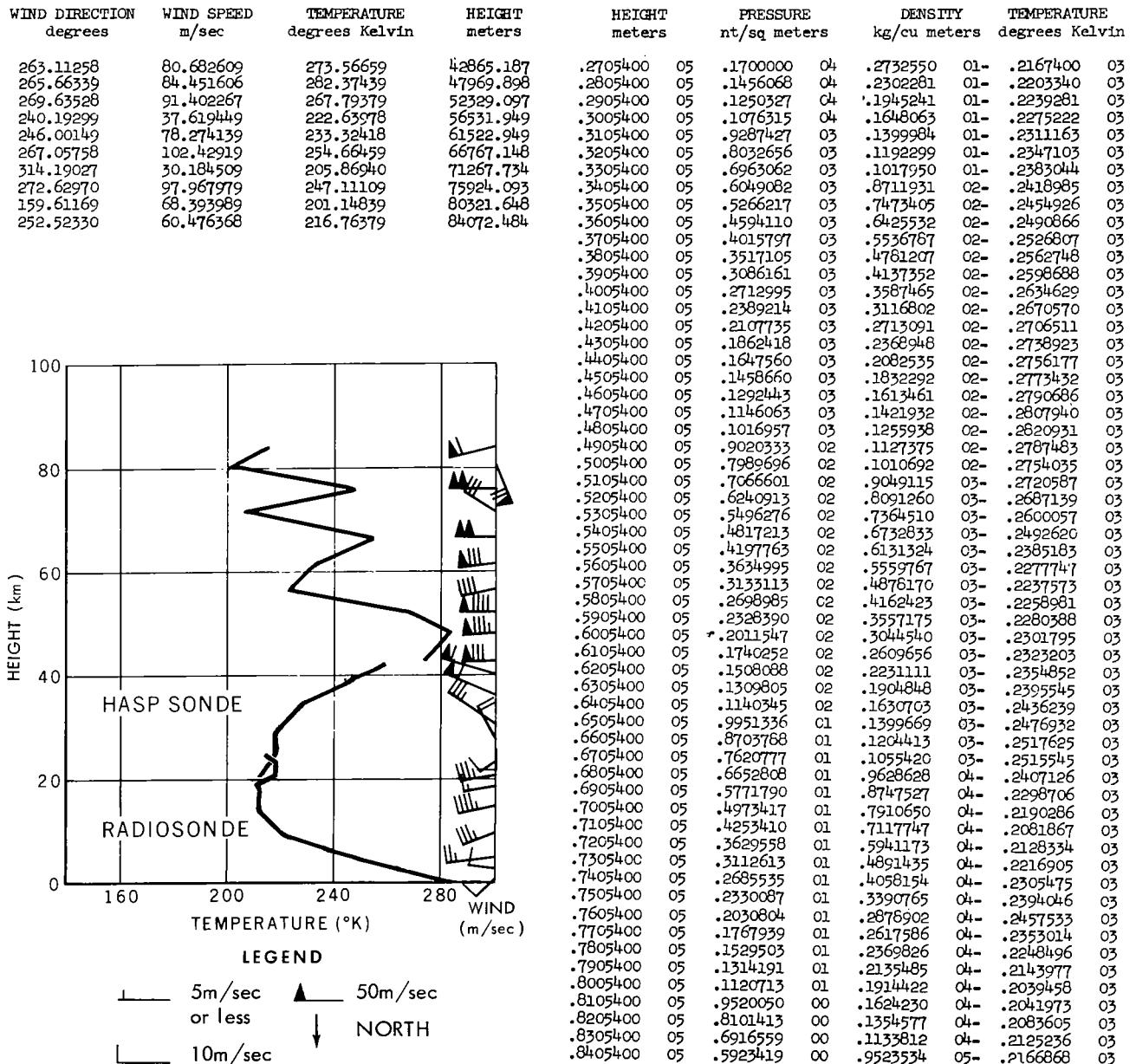


FIGURE 24
28 FEBRUARY 1963, 1548 CST FT. CHURCHILL

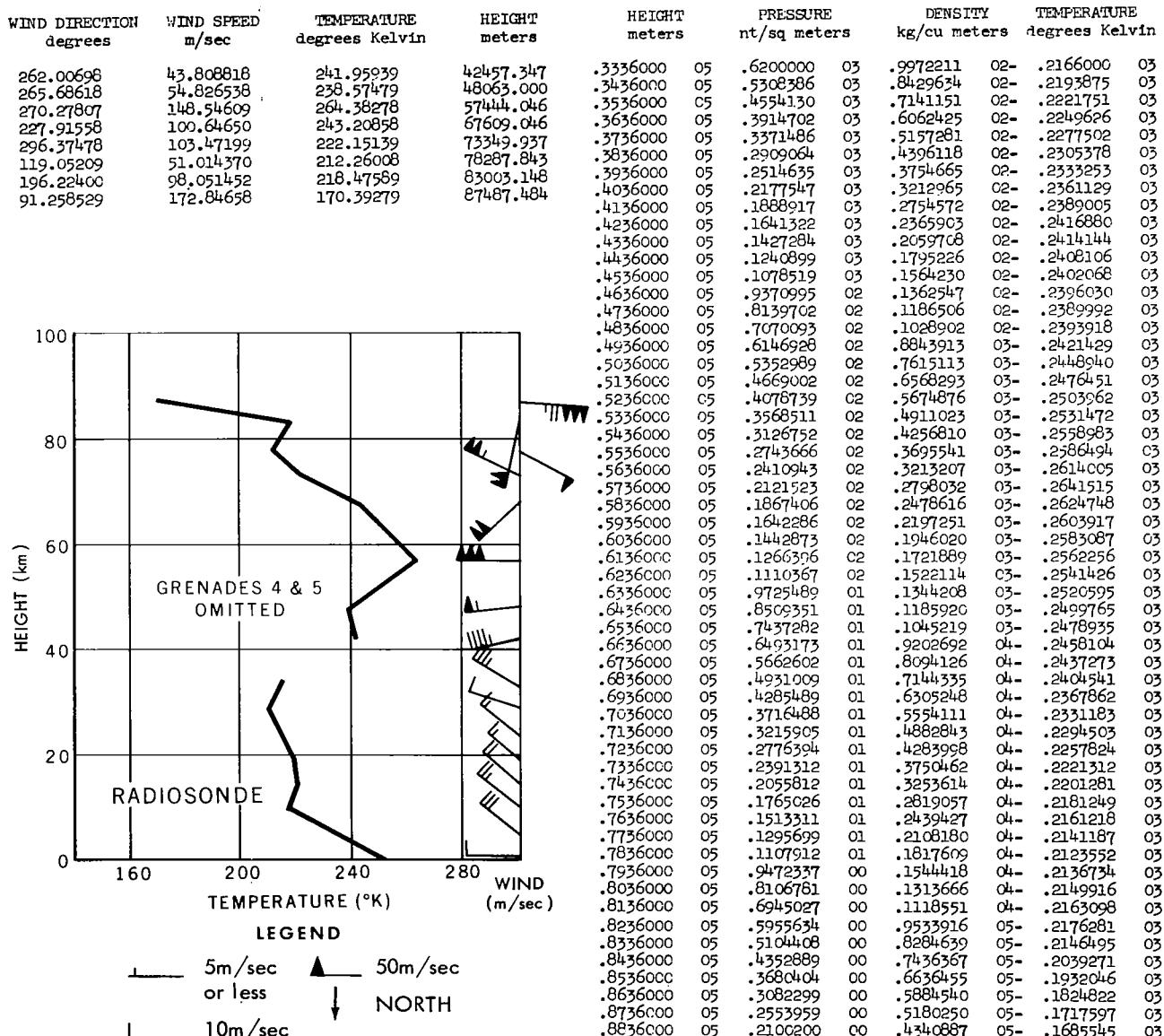


FIGURE 25
28 FEBRUARY 1963 1711 EST, WALLOPS ISLAND, VA

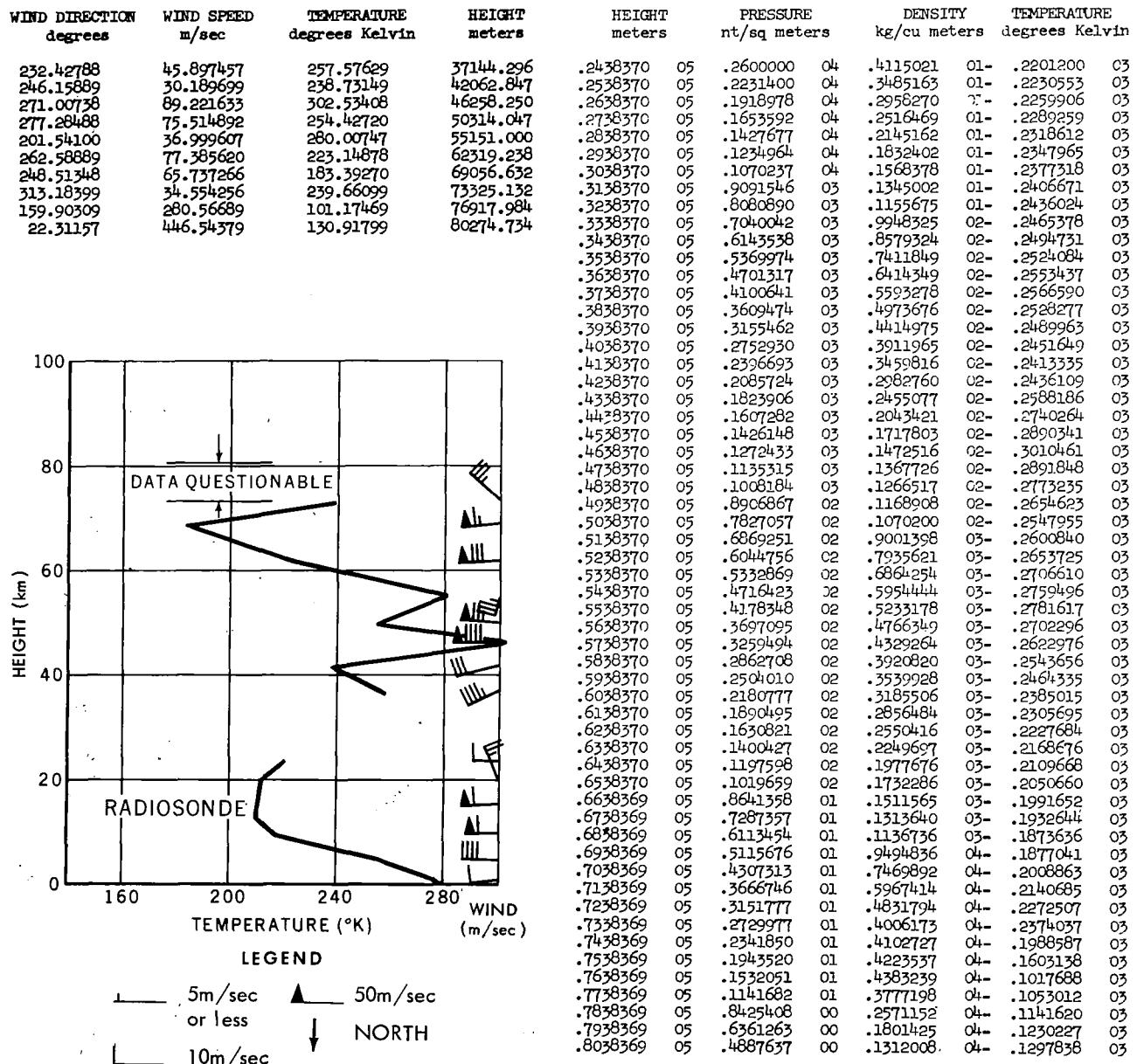


FIGURE 26
8 MARCH 1963, 1801 CST FT. CHURCHILL

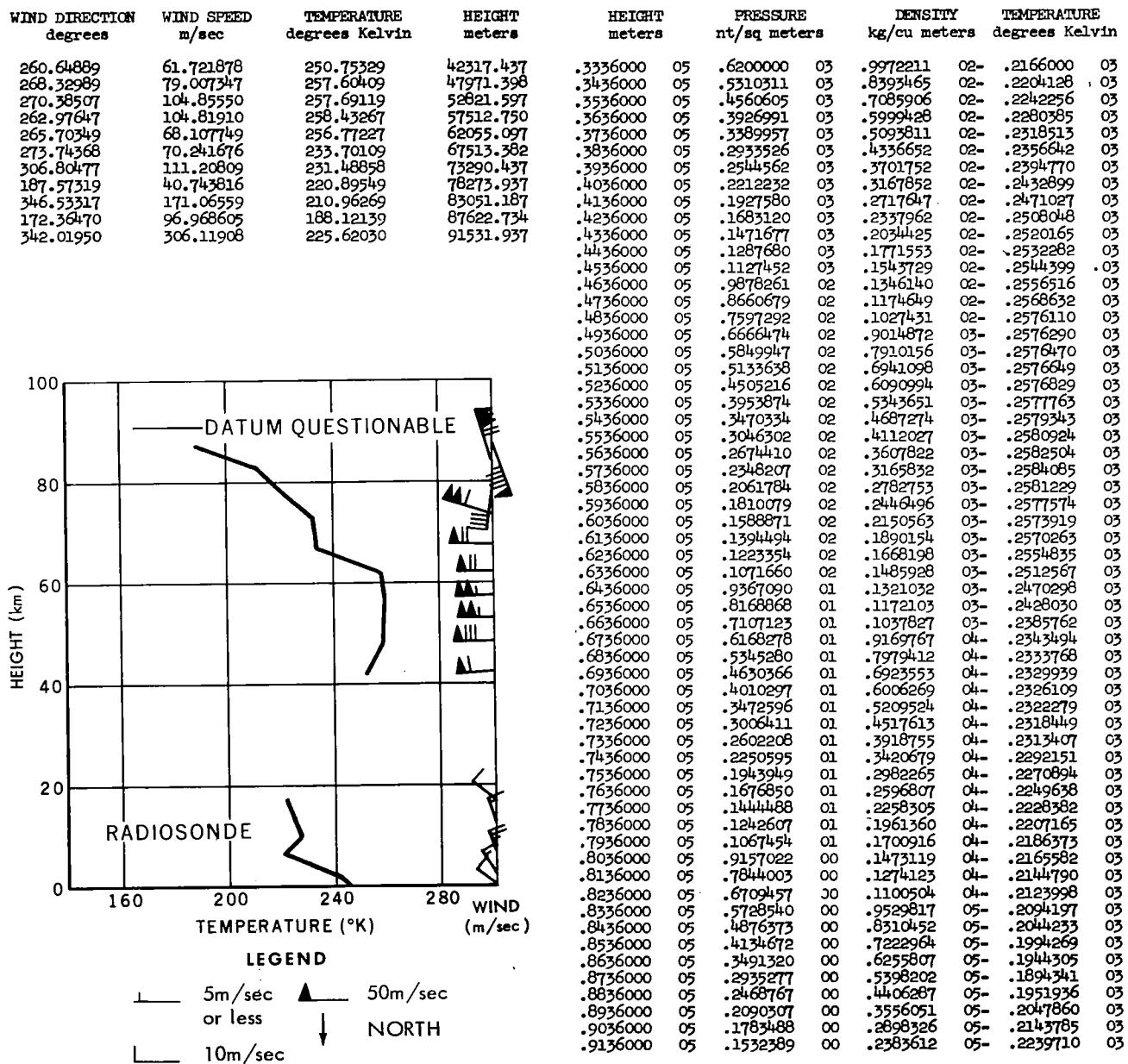


FIGURE 27
8 MARCH 1963, 1901 EST, WALLOPS ISLAND, VA.

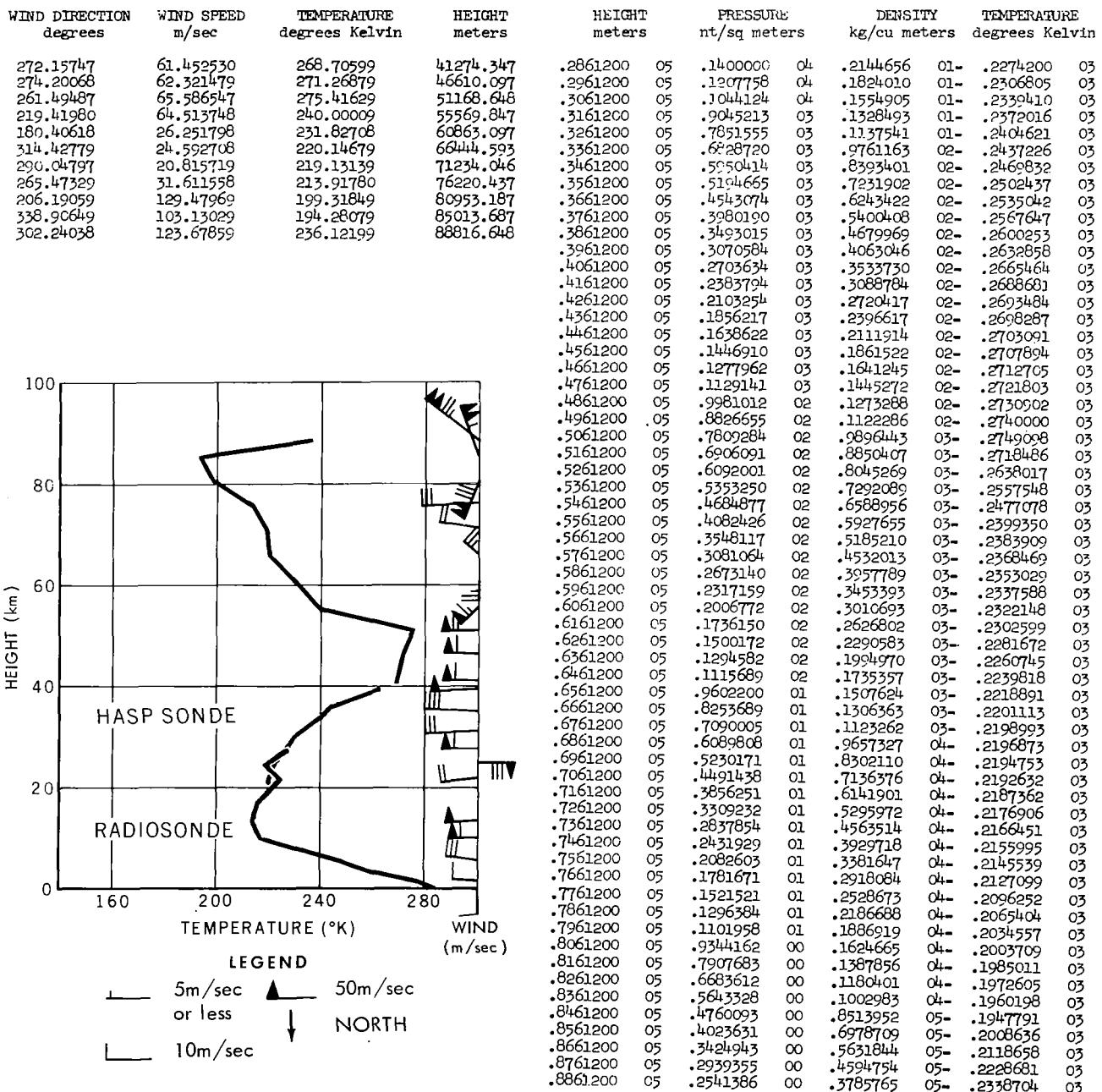
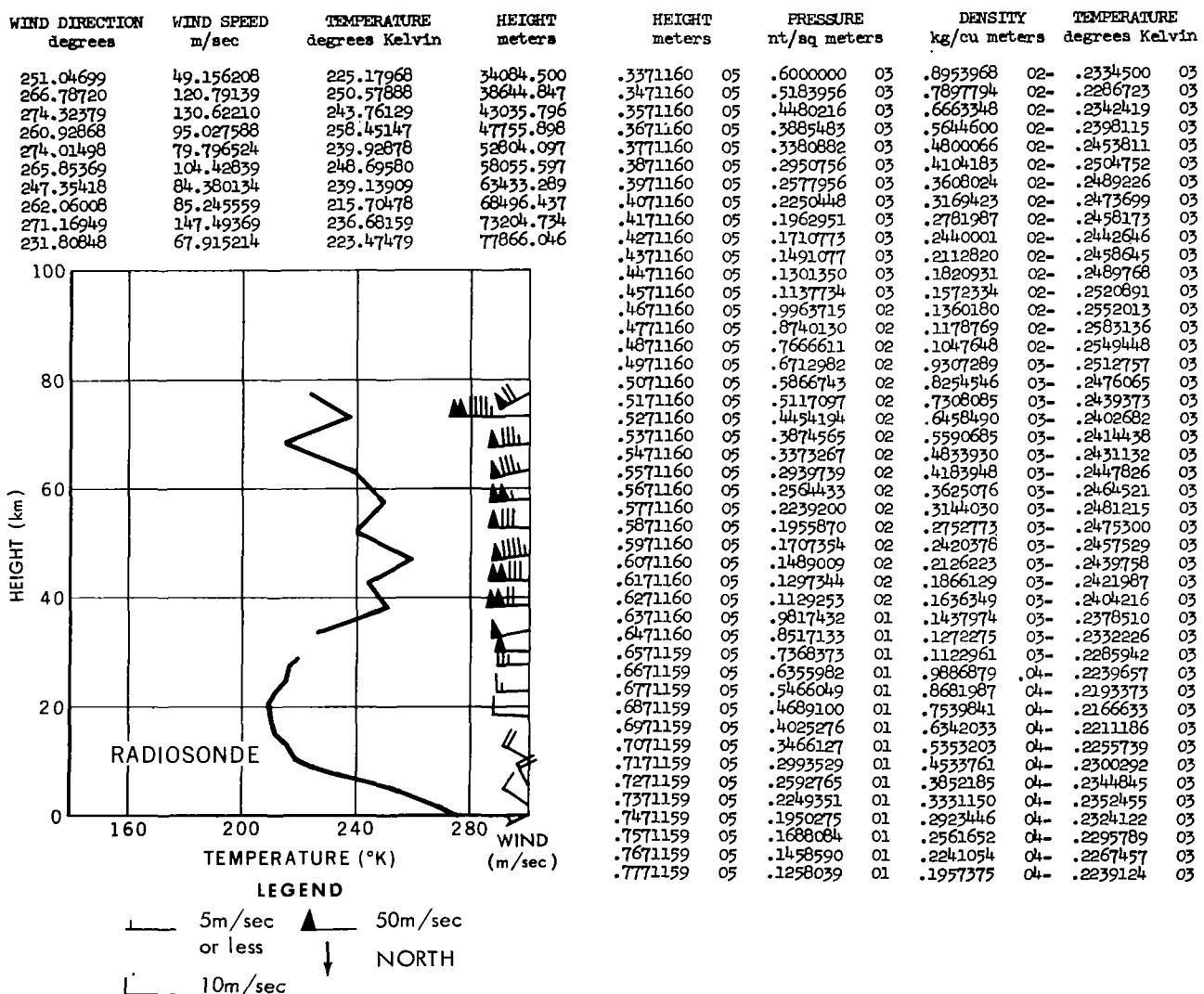


FIGURE 28
7 DECEMBER 1963, 0811 EST, WALLOPS ISLAND, VA.



Figures 29 through 38
Temperature and wind error functions for the rocket
grenade experiment of June 7, 1962, obtained with the
aid of a digital computer.

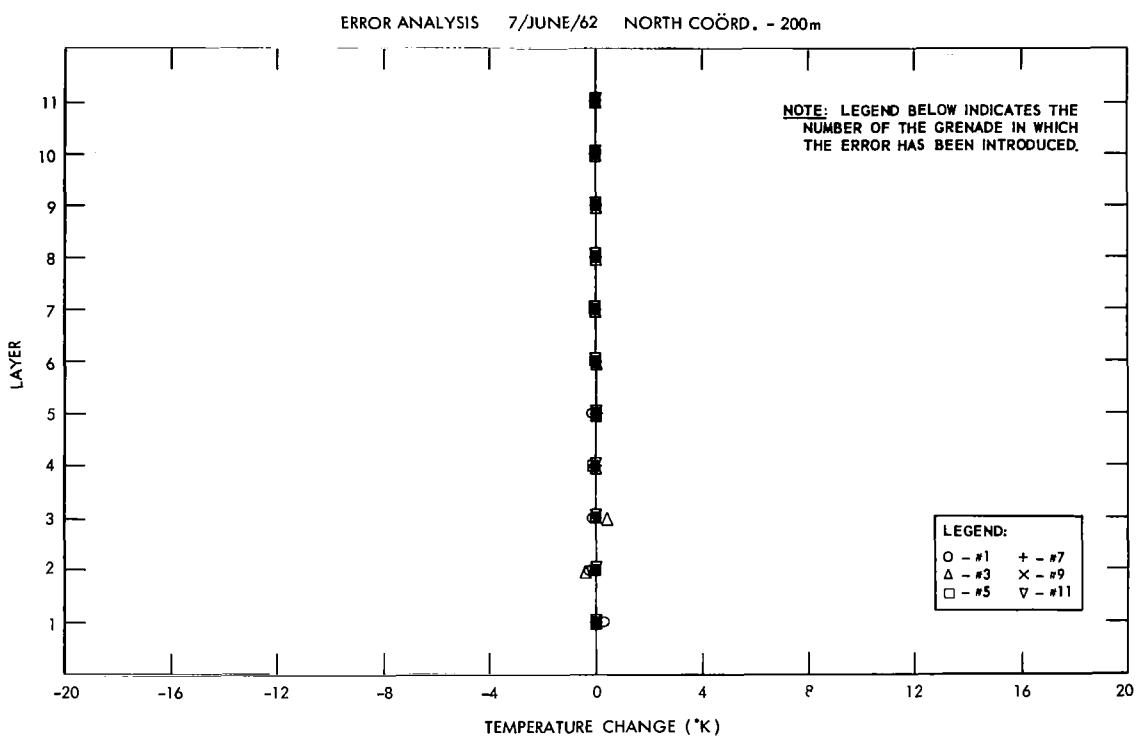


FIGURE 29

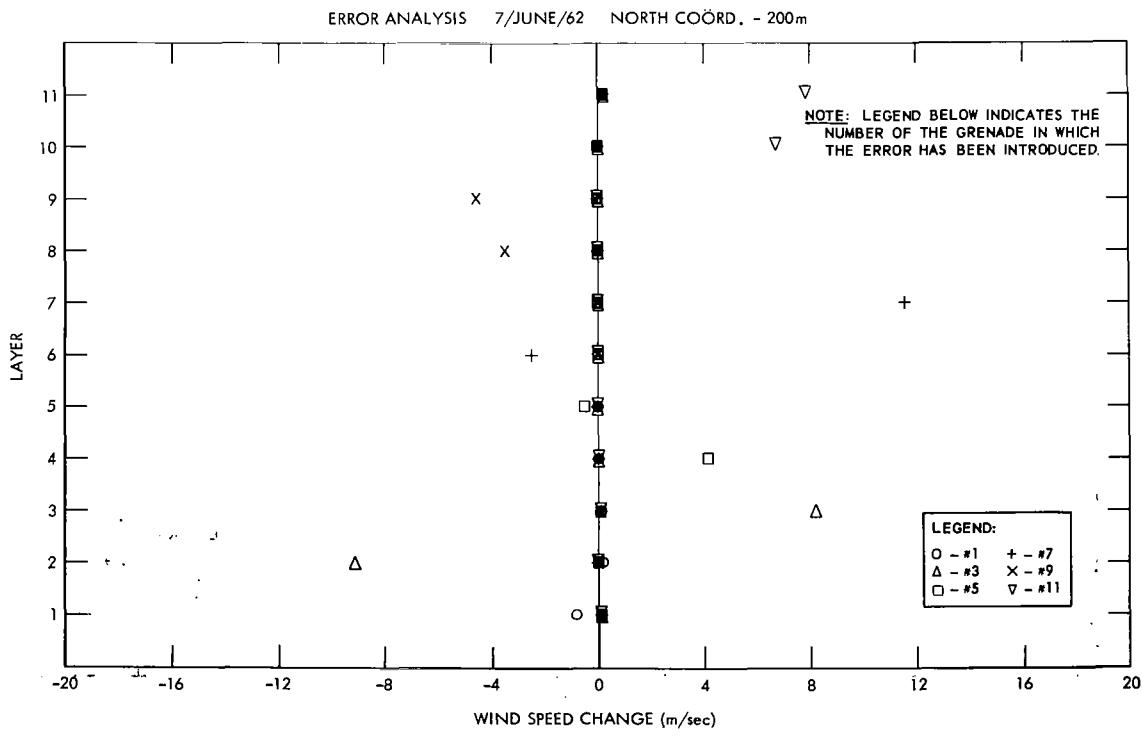


FIGURE 30

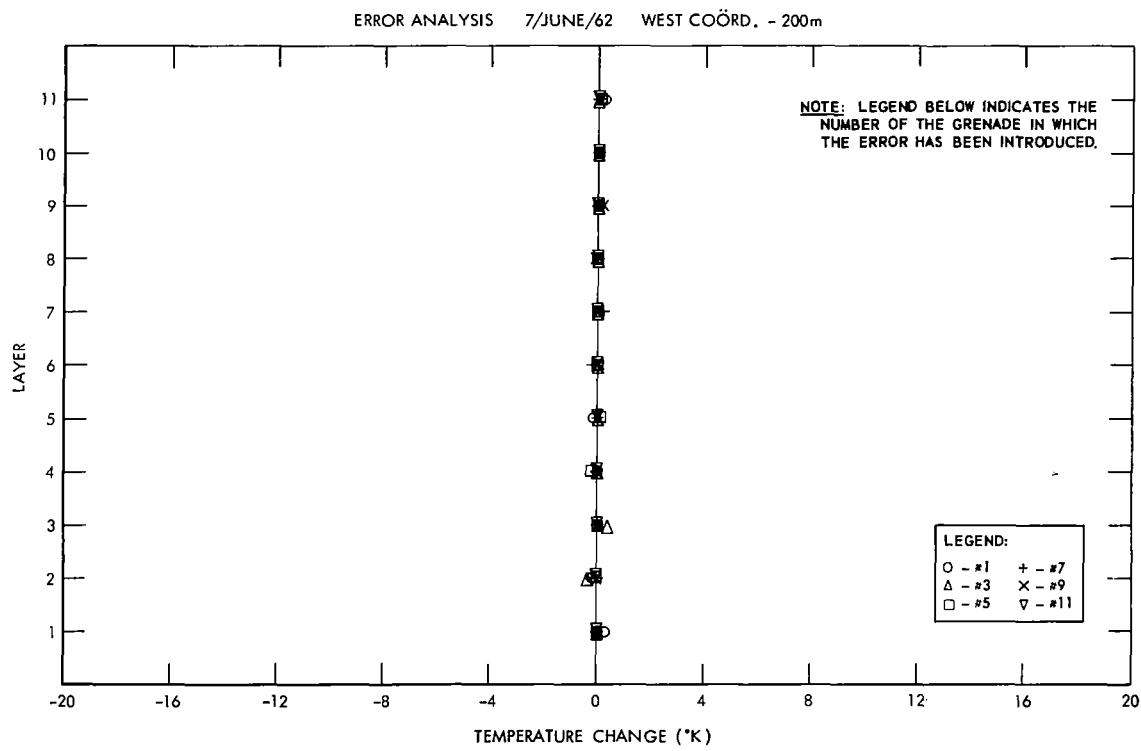


FIGURE 31

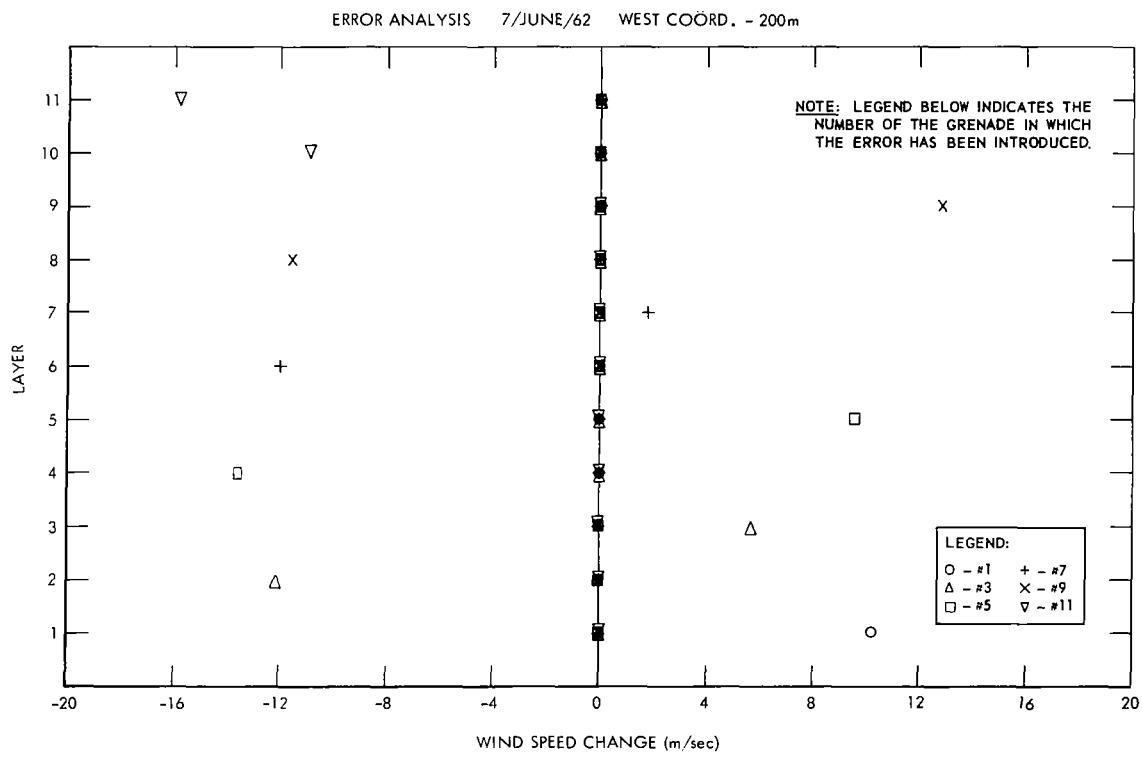


FIGURE 32

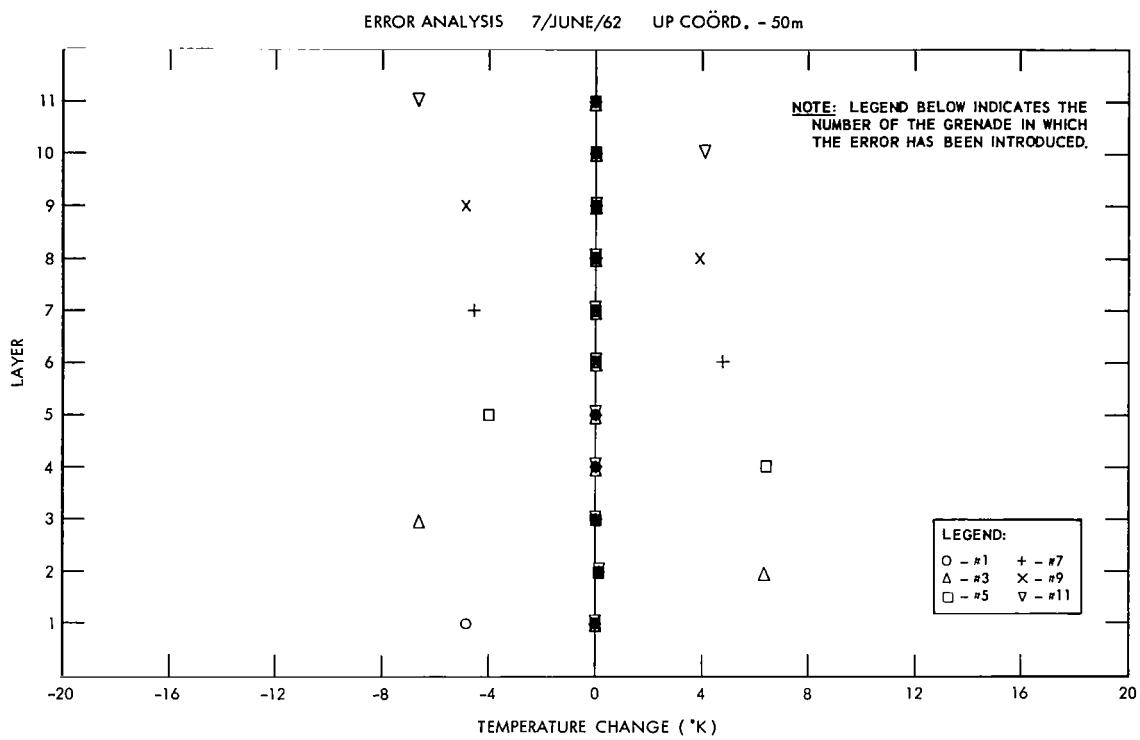


FIGURE 33

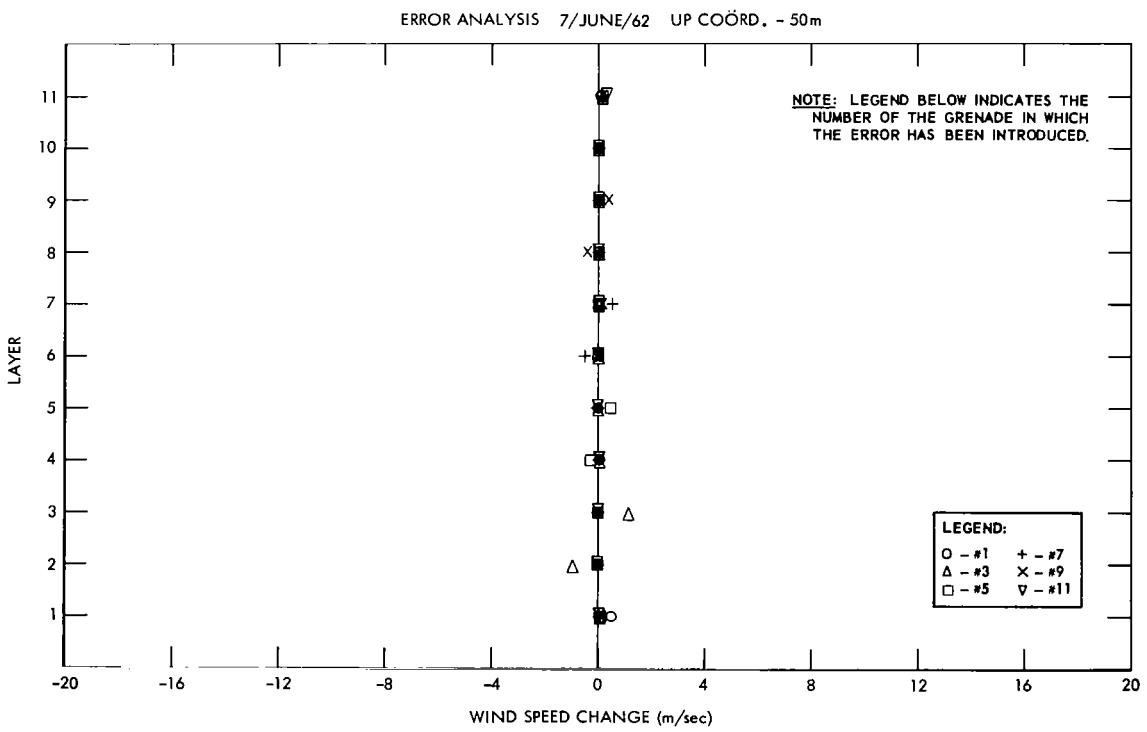


FIGURE 34

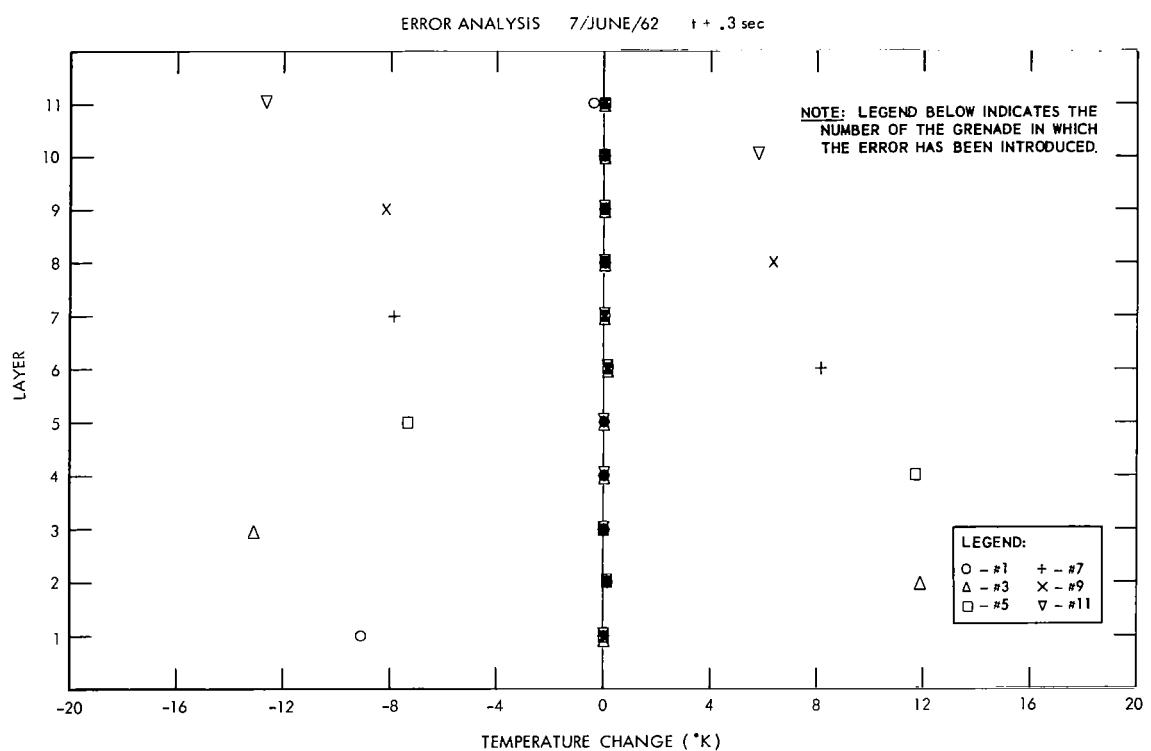


FIGURE 35

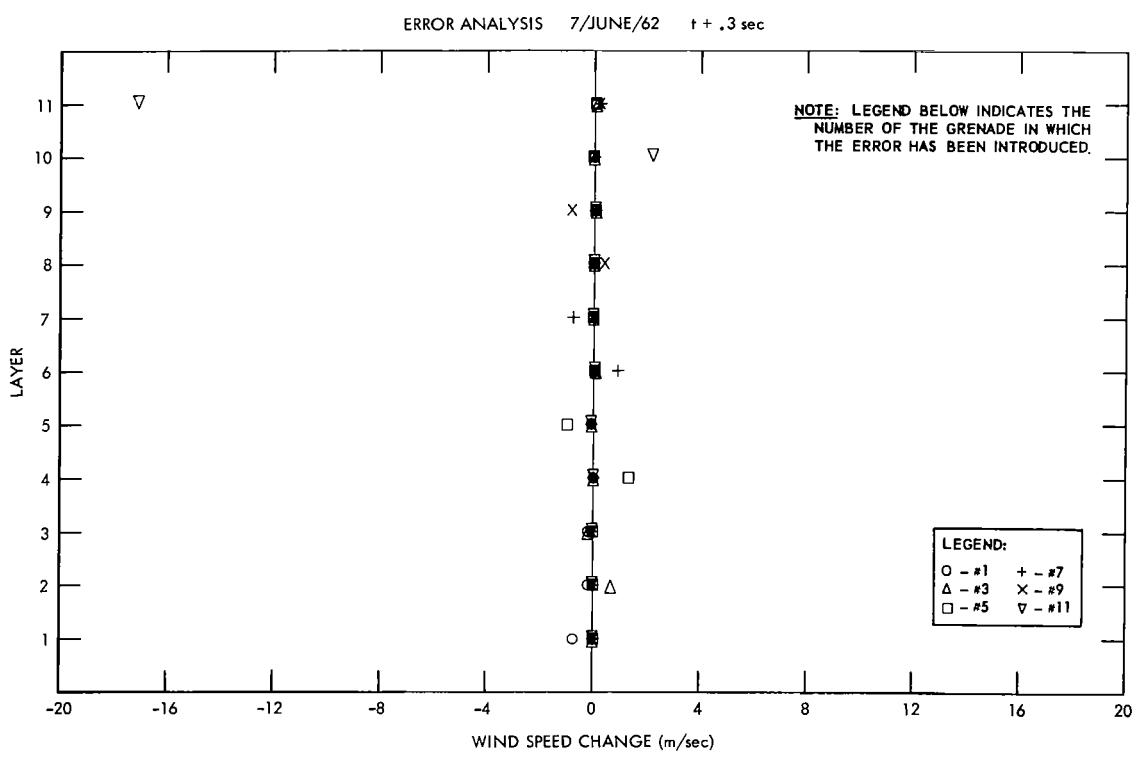
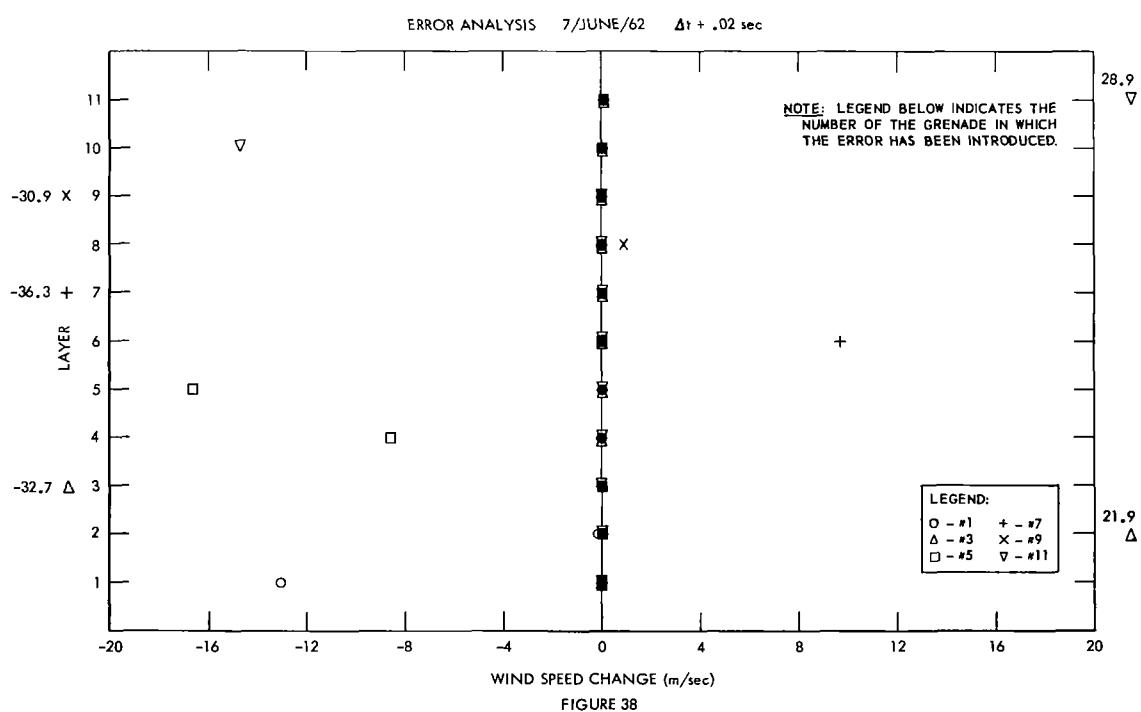
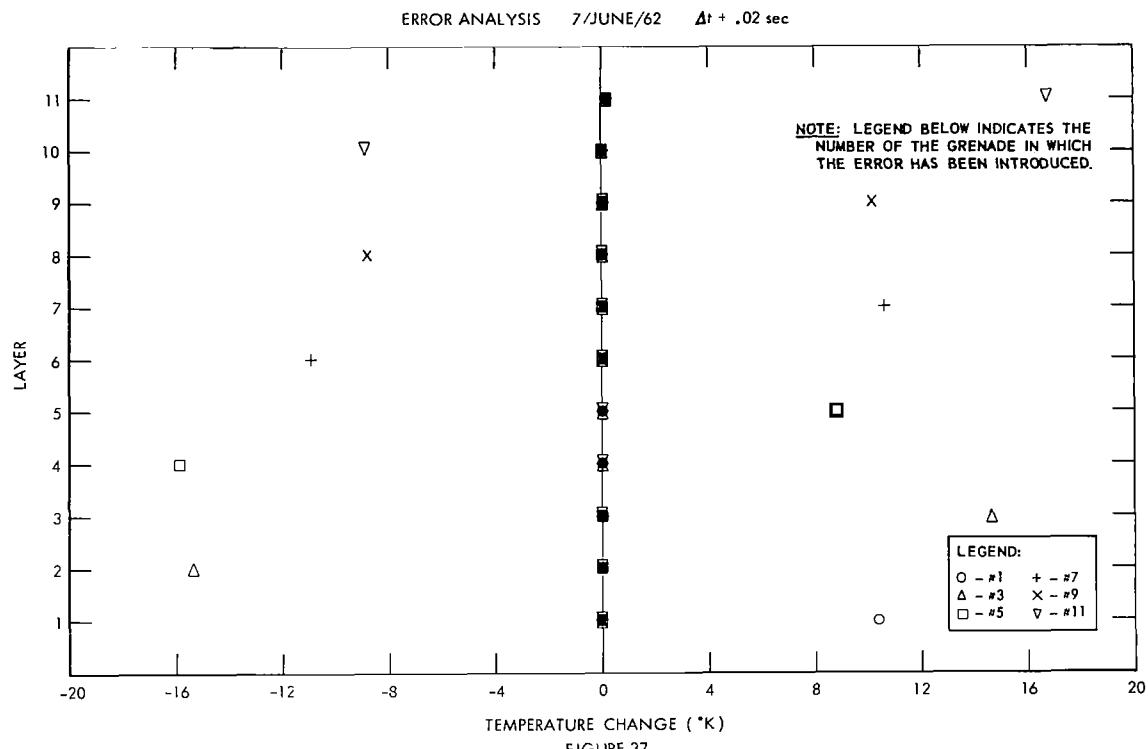


FIGURE 36



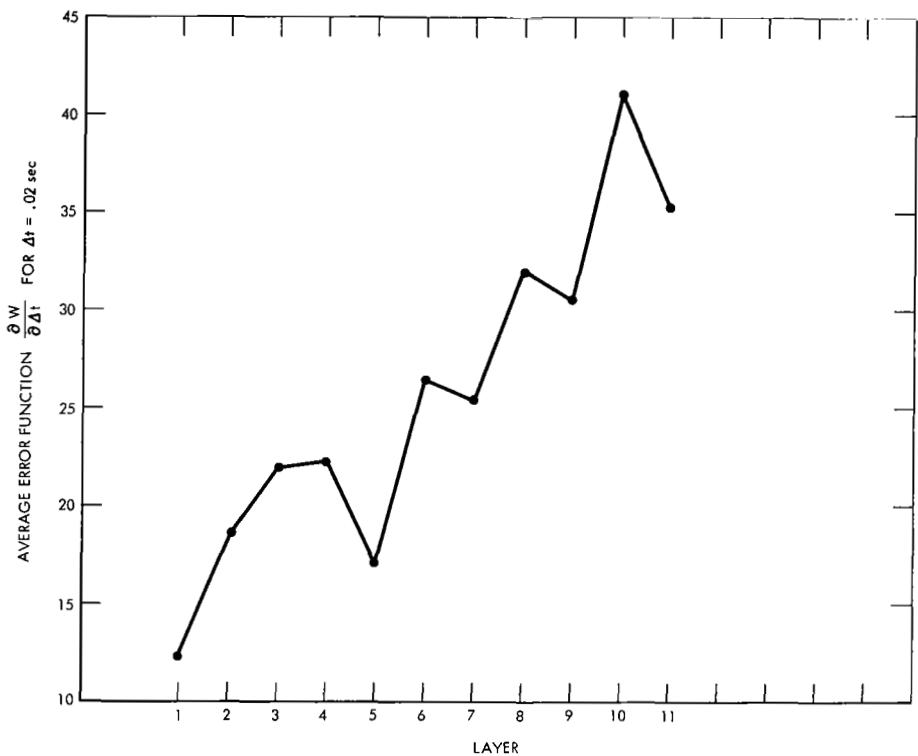


Figure 39—Graph of $\partial W / \partial \Delta t$ vs. layer, for $\Delta t = .02$ sec (average for 16 firings).

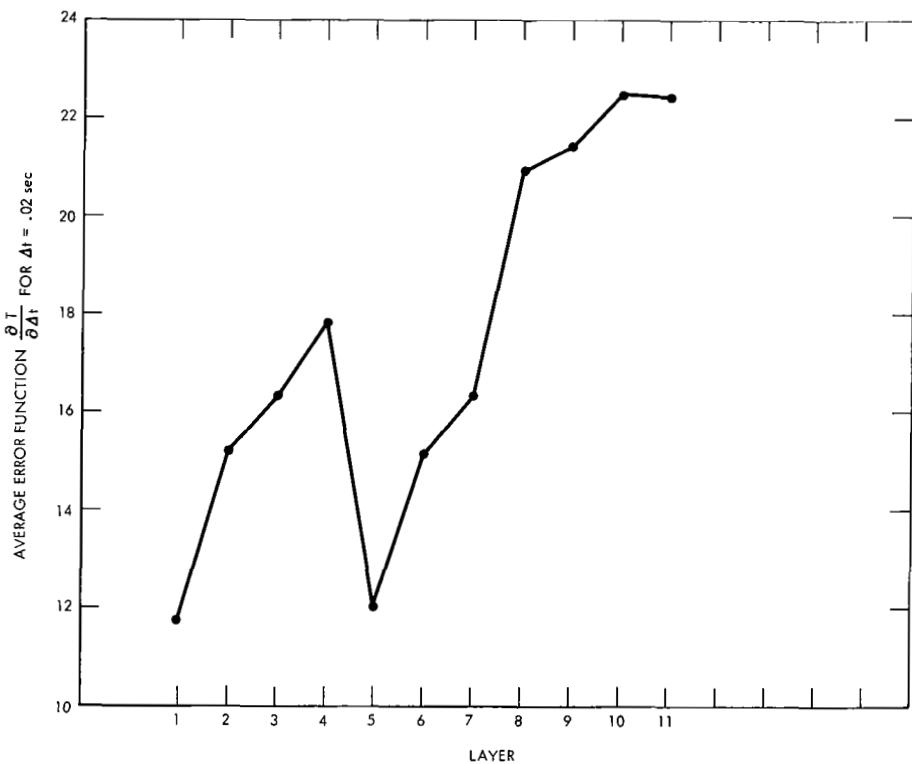


Figure 40—Graph of $\partial T / \partial \Delta t$ vs. layer, for $\Delta t = .02$ sec (average for 16 firings).

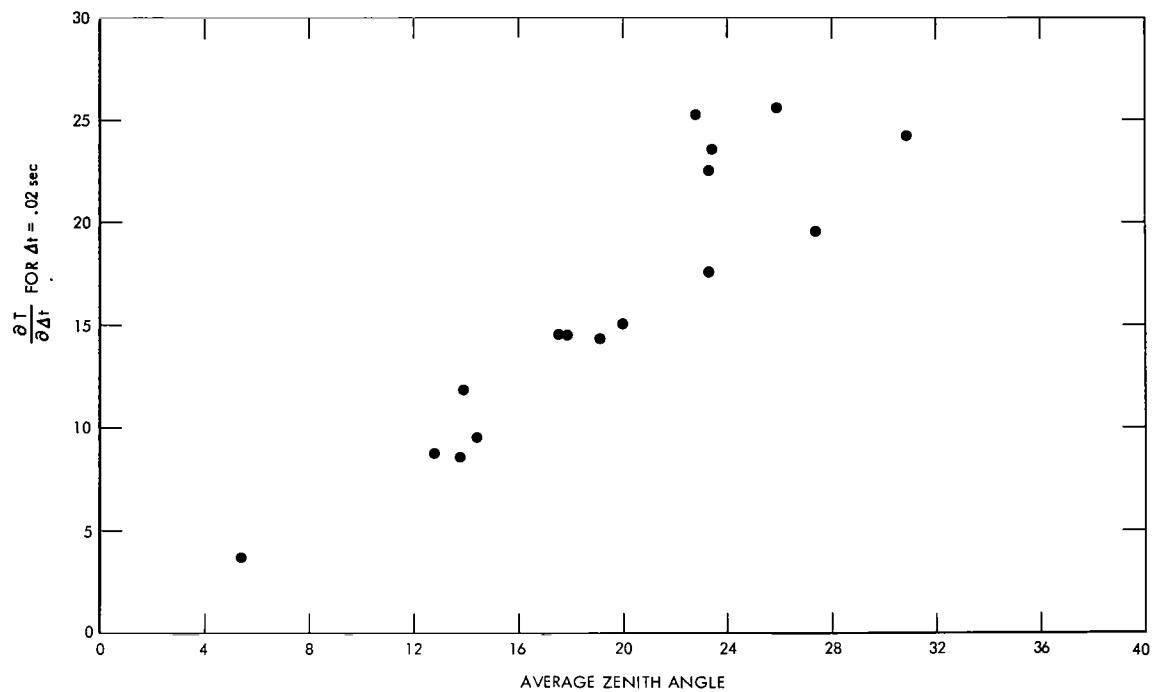


Figure 41—Dependence of $\partial T / \partial \Delta t$ upon zenith angle, for $\Delta t = .02$ sec (average for 16 firings).

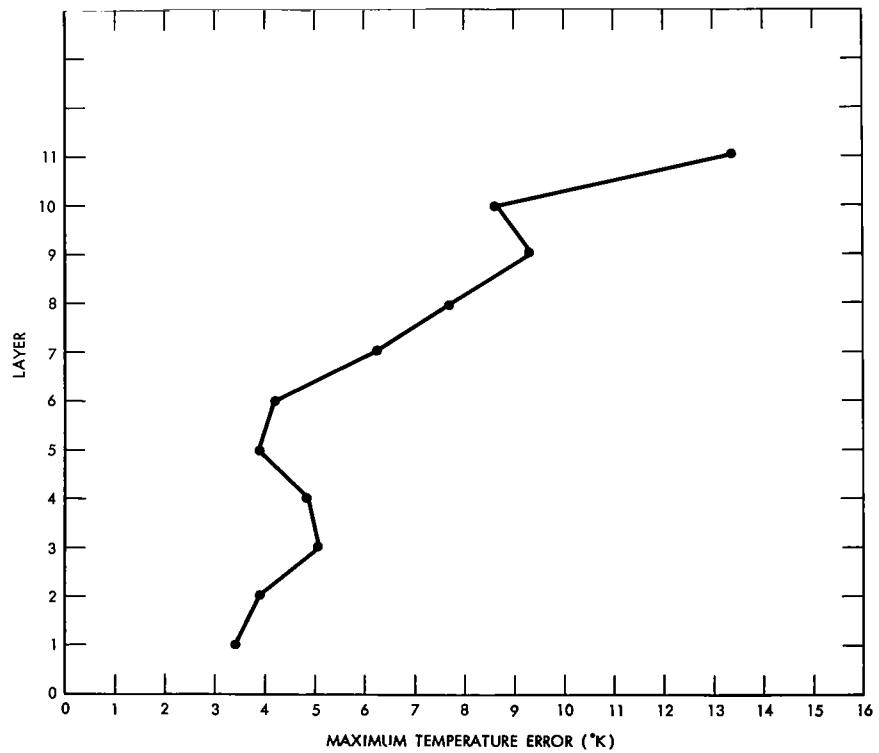


Figure 42—Maximum temperature errors for the 16 firings, 1960-1963.

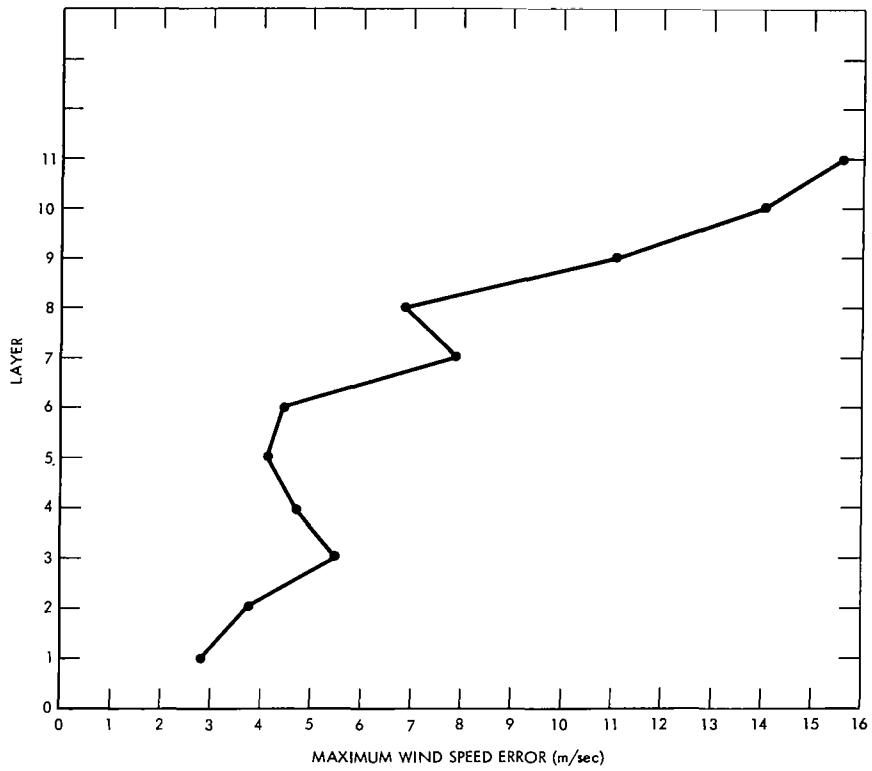


Figure 43—Maximum wind errors for the 16 firings, 1960-1963.

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